

STUDY OF THE DYNAMICS OF FLUX TRAPPING IN DIFFERENT SRF MATERIALS

F. Kramer, S. Keckert, O. Kugeler, J. Knobloch, T. Kubo

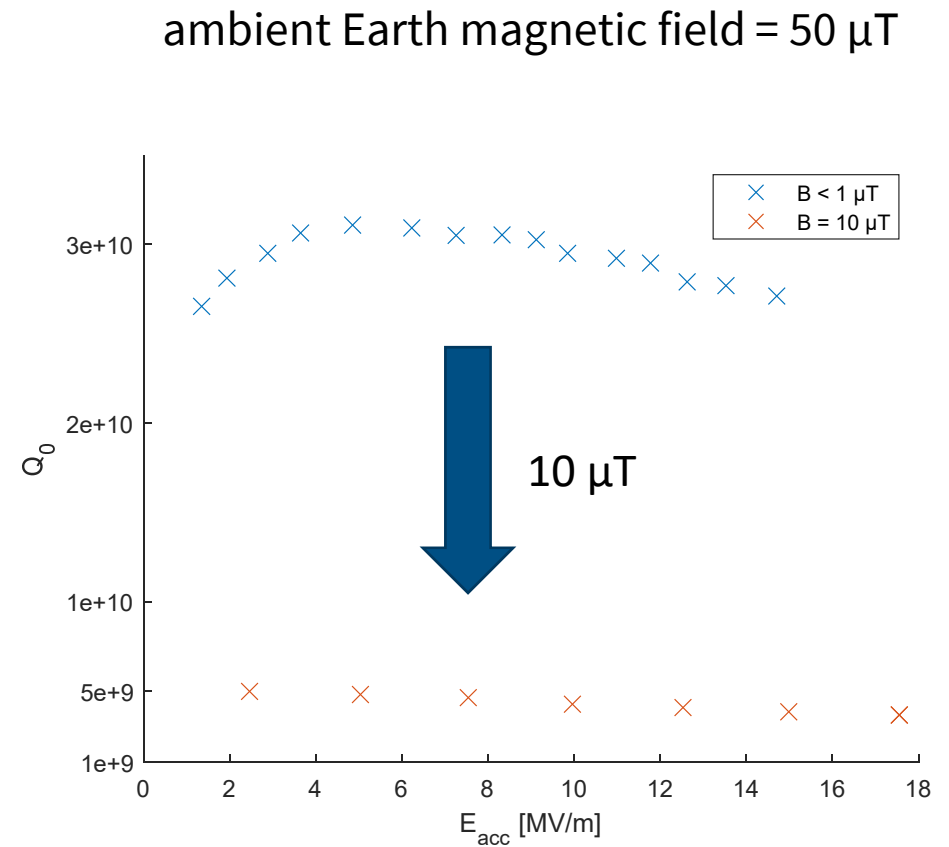
SRF 2023

SRF

Grand Rapids,
USA

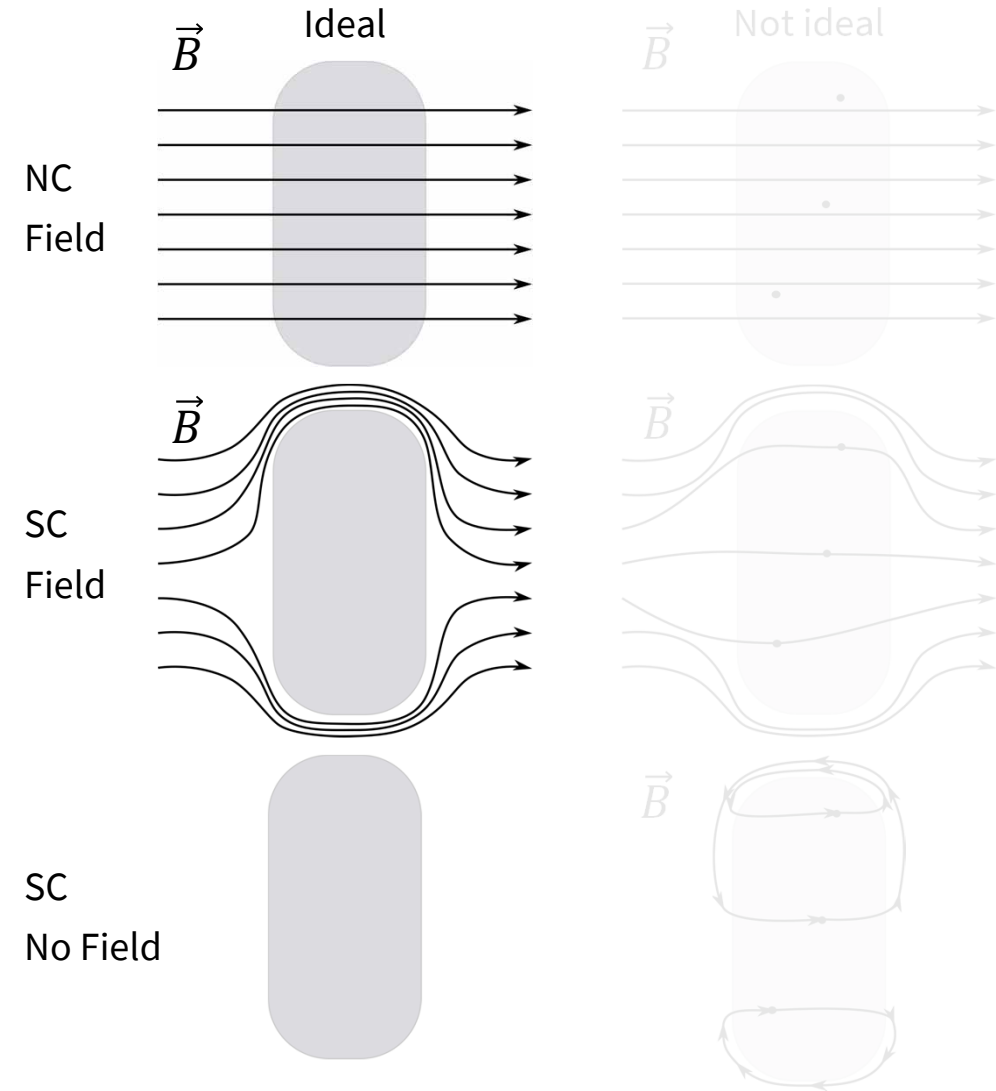
Brief recap: Why do we care about trapped flux?

- Trapped flux reduces Q_0 in SRF cavities
- Double magnetic shielding reduces ambient Earth magnetic field from $50 \mu\text{T}$ to $< 1 \mu\text{T}$
- But it is impossible to completely shield off all magnetic fields
- Magnetic shielding is expensive
- Shielding does not reduce intrinsic fields caused by thermo currents
- Find a way to reduce flux trapping efficiency



Trapped Flux: What is it?

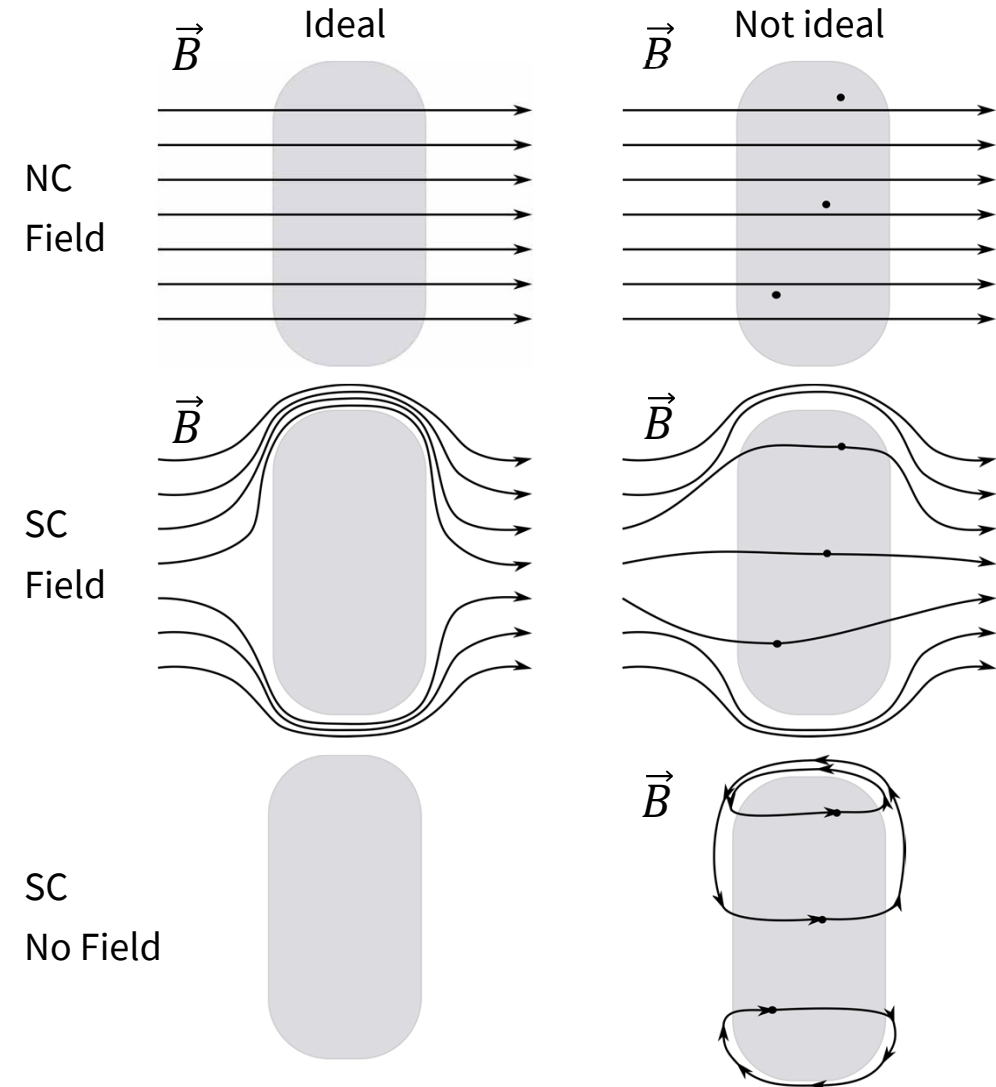
- When cooling down a Type I superconductor in an external magnetic field, it will transition into the *Meissner* state. In this state all magnetic field is expelled.
- However, there are small defects in the material which *pin* the quantized magnetic field lines and prevent them from being pushed out
- The pinned flux lines oscillate in the RF field and cause losses in the cavity wall [1]



[1] Gurevich, A. and Ciovati, G., Effect of vortex hotspots on the radio-frequency surface resistance, *Phys. Rev. B*, 2013

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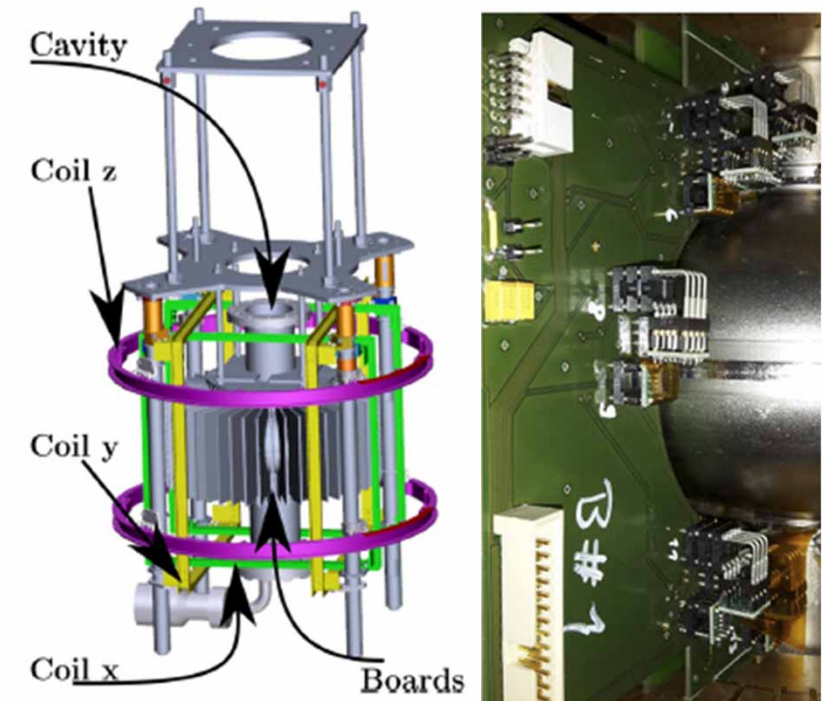
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CONCEPT – USE FLAT SAMPLES

- We want to understand trapped flux in more detail, before trying to minimize it
- To understand trapped flux, we need control parameters which might have an influence on it:
 - Temperature gradient
 - Cooldown rate
 - Ambient magnetic field
 - Impact of geometry (demagnetization factor, shape anisotropy)
 - Material & treatment

Use samples instead of cavities

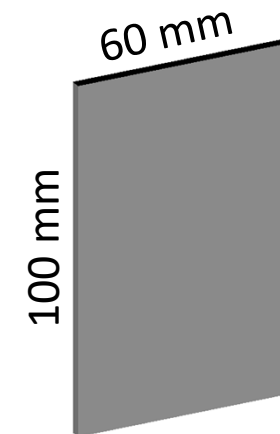
- Better Control of the parameters
- More cooling cycles possible ($\sim 300/\text{day}$ instead of $\sim 3-4/\text{day}$)
- Less material needed and treatments are easier to apply
- Easier geometry



AMR based magnetometry system developed at HZB for cavities in 2017 $\sim 3-4$ cycles per day



Investigate Nb sheets
 ~ 300 cycles per day



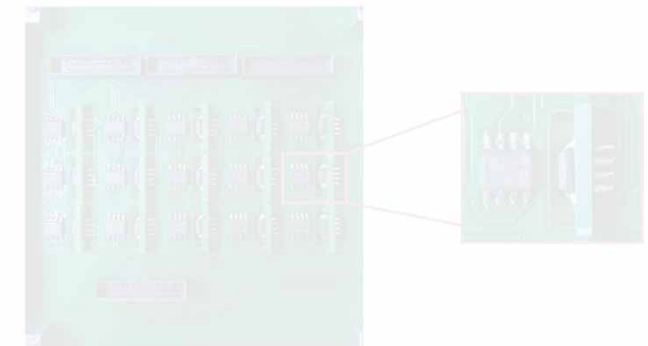
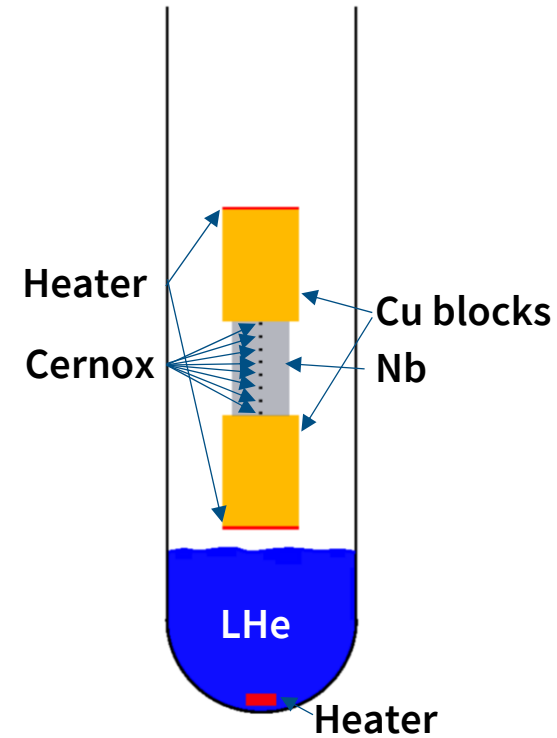
EXPERIMENTAL INFRASTRUCTURE

- Small glass cryostat
- Filled from helium Dewar
- No magnetic shielding
- **Active field compensation** with two Helmholtz coils and one solenoid
- Minimum flux density at location of reference sensors: $< 15 \text{ nT}$
(Earth magnetic field $\sim 50 \mu\text{T}$)
- Maximum flux density: $190 \mu\text{T}$



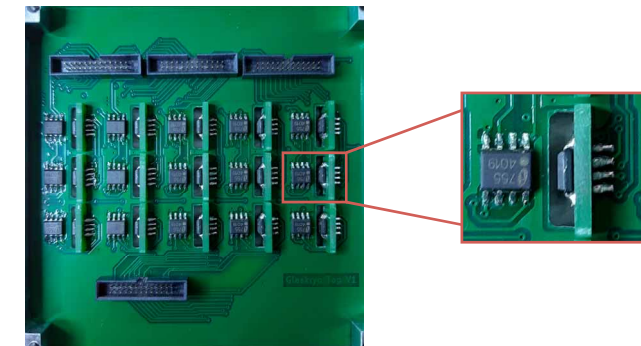
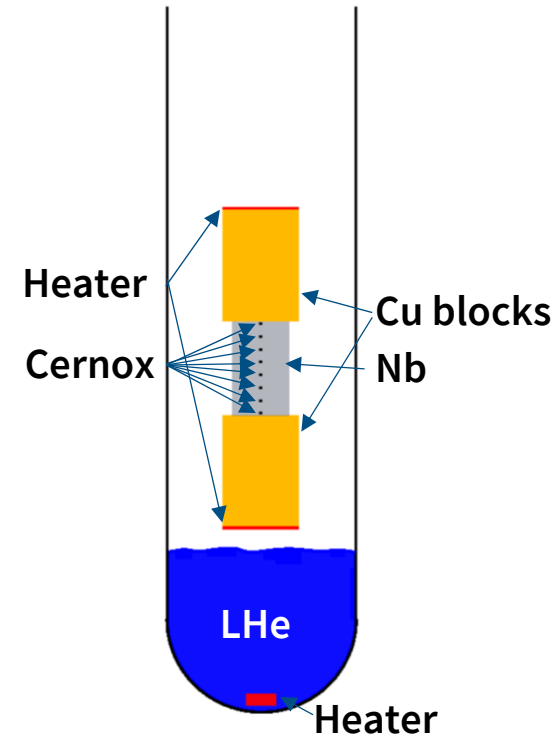
EXPERIMENTAL SETUP

- Sample (100x60x3)mm, clamped in copper blocks at either end
- Dual heaters on the end of the blocks allow for precise control of **temperature gradient** and **cooldown rate**
- Blocks move electric heaters away from sample, this reduces magnetic fields from the heaters at the sample
- Setup is suspended above liquid helium bath
- Heater in helium is used to control helium gas flow
- 8 Cernox sensors measure temperature distribution across sample
- Multiple AMR sensors for magnetic field measurements
- grouping of 3 sensors to measure field vector in 3d
- 15 AMR sensor groups measure magnetic field just above the sample



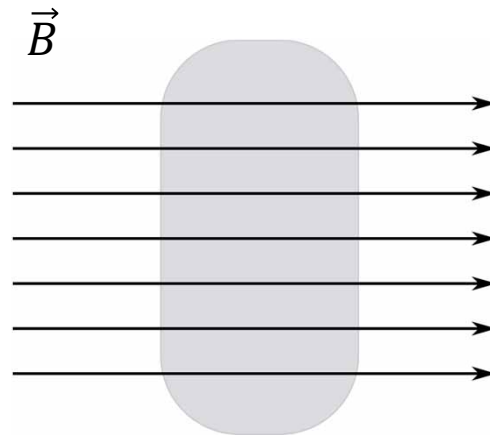
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A TYPICAL COOLDOWN

- Apply external field $B_{\text{ext}} = 100 \mu\text{T}$
- Set Temperature gradient across sample ($\nabla T = 0.06 \text{ K/cm}$)
- Lower Sample temperature at top and bottom simultaneously
- After Sample is fully superconducting, remove external field $B_{\text{ext}} = 0 \mu\text{T}$
- Measure trapped flux

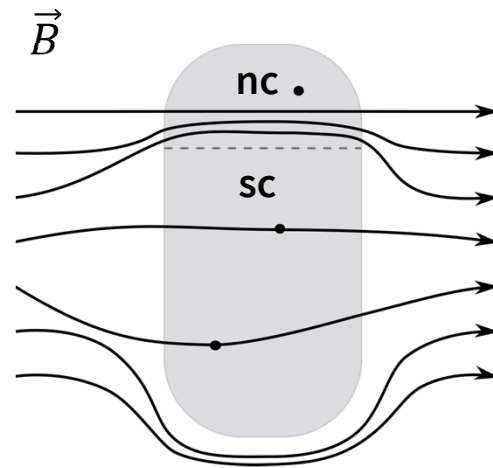


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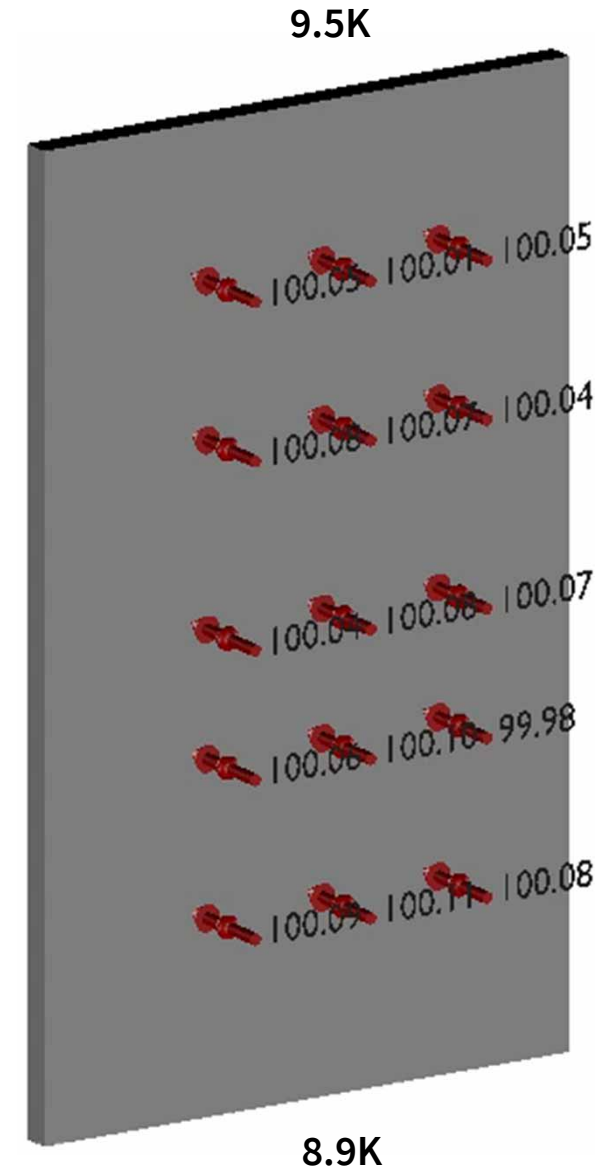
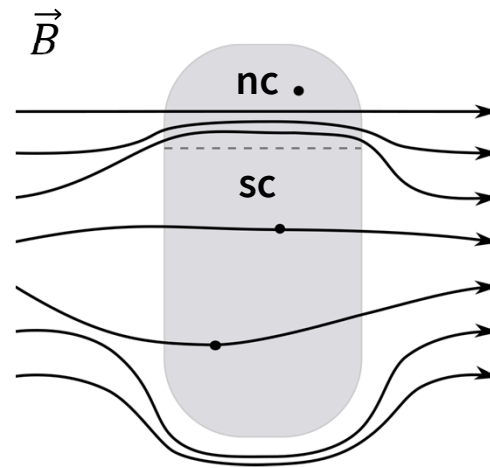


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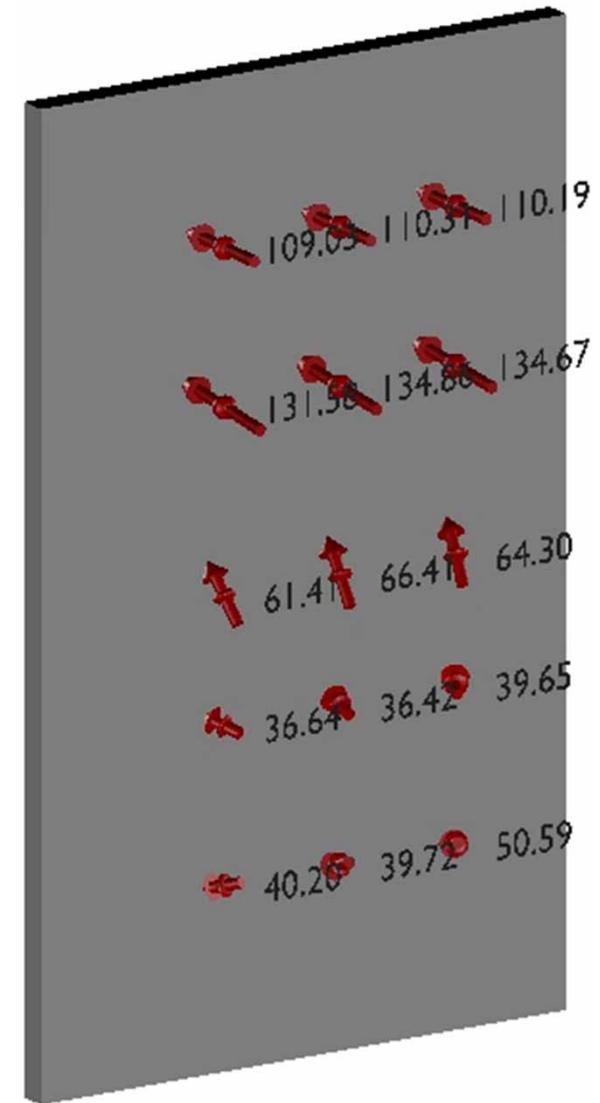
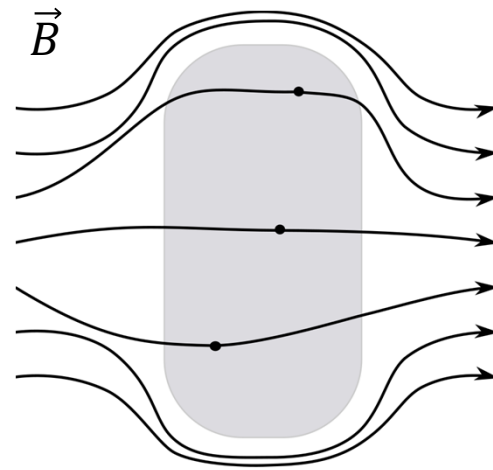
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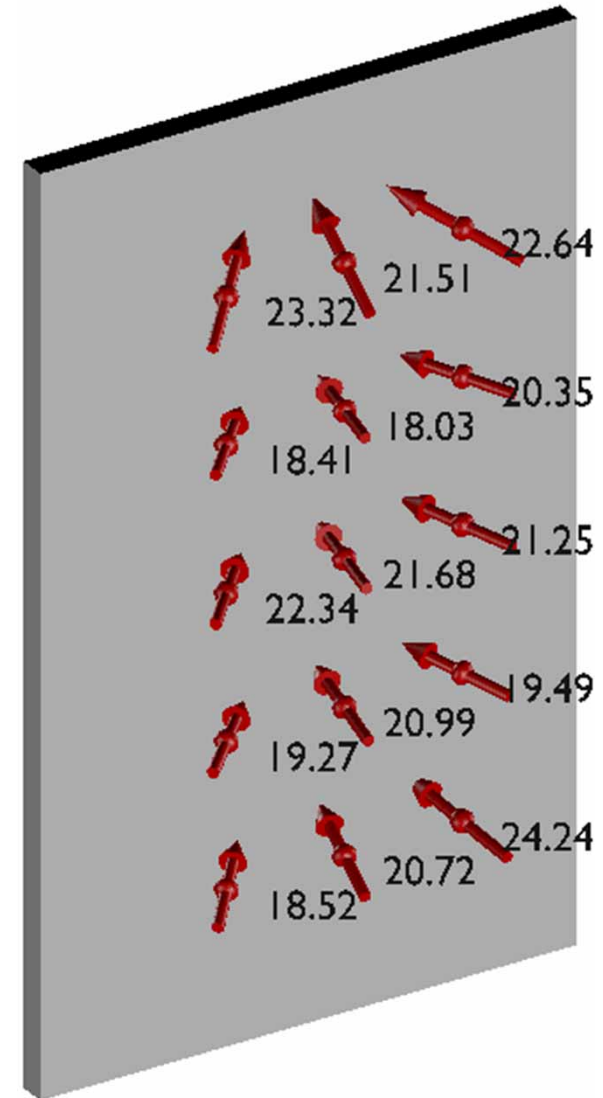
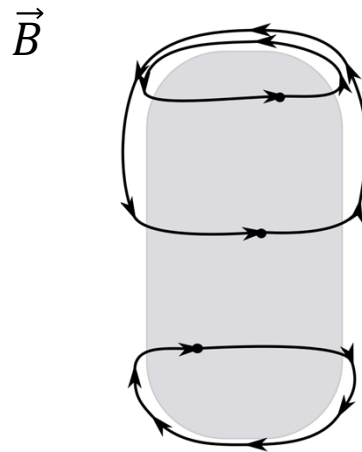
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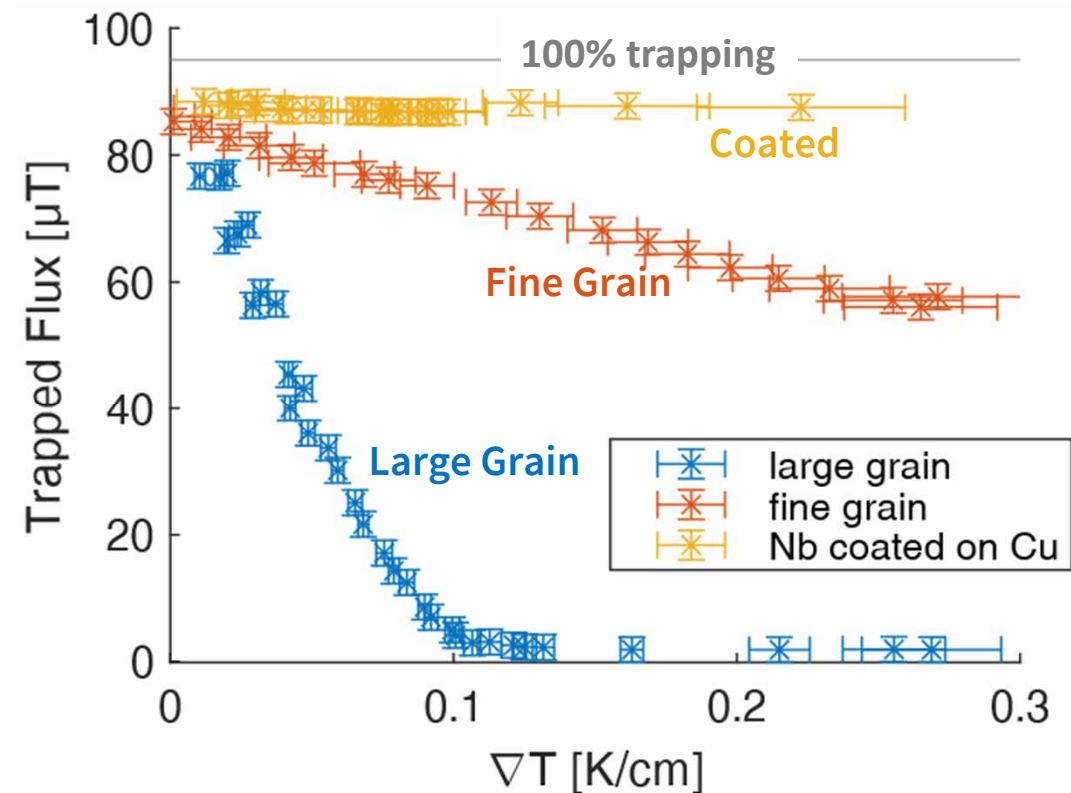
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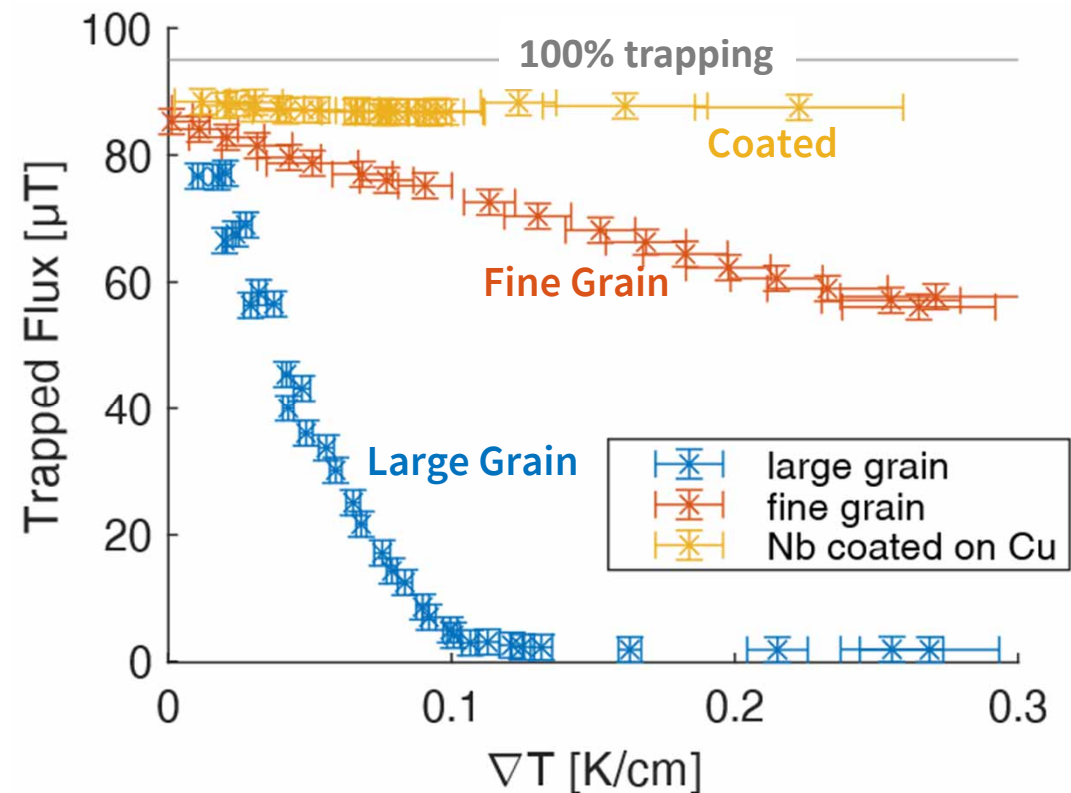
TRAPPED FLUX VS TEMPERATURE GRADIENT

- Vary temperature gradient while keeping external magnetic field and cooldown rate constant
 - $B_{\text{ext}} = 100 \mu\text{T}$
 - $dT/dt = 0.07 \text{ K/s}$
- Comparison of three samples
 - Nb large-grain (untreated)
 - Nb fine-grain (untreated)
 - Nb coated on Cu ($4 \mu\text{m}$)
- Less trapped flux with higher temperature gradient
- Large grain material allows near 100% flux expulsion
- No effect for coated sample



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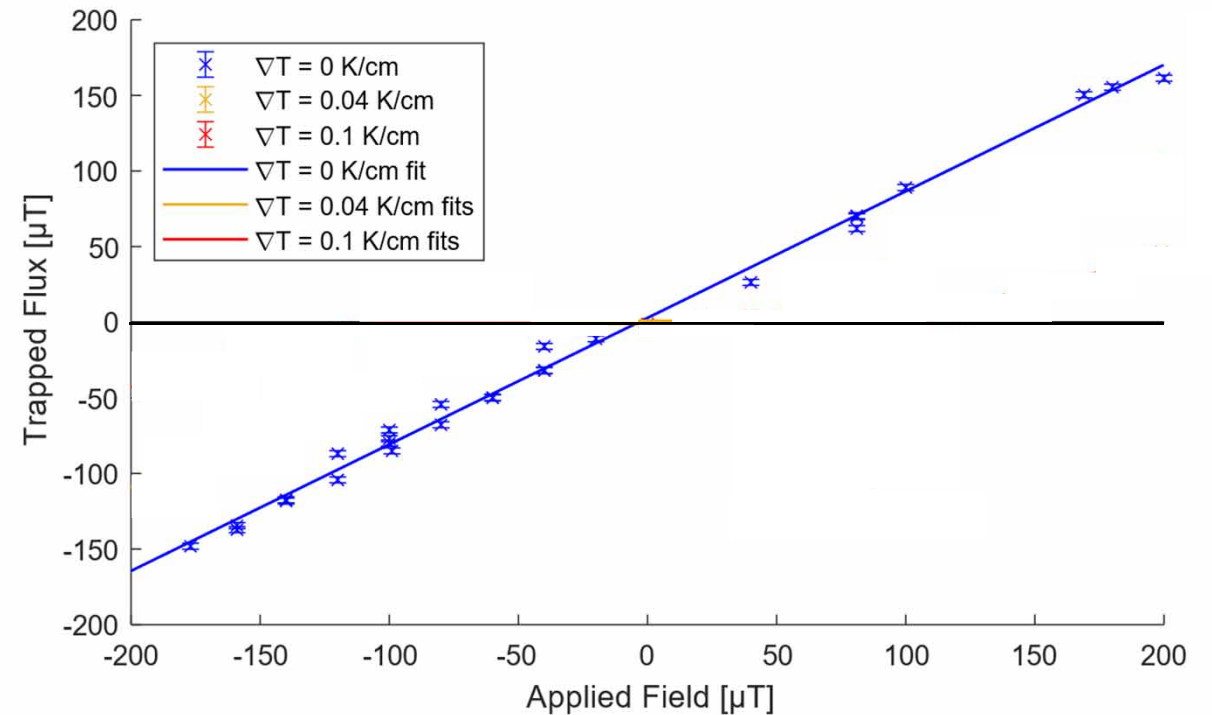


Nearly full expulsion with untreated large-grain
Thin film is sufficient to have nearly full trapping

TRAPPED FLUX VS AMBIENT FIELD

Large-grain Nb sample

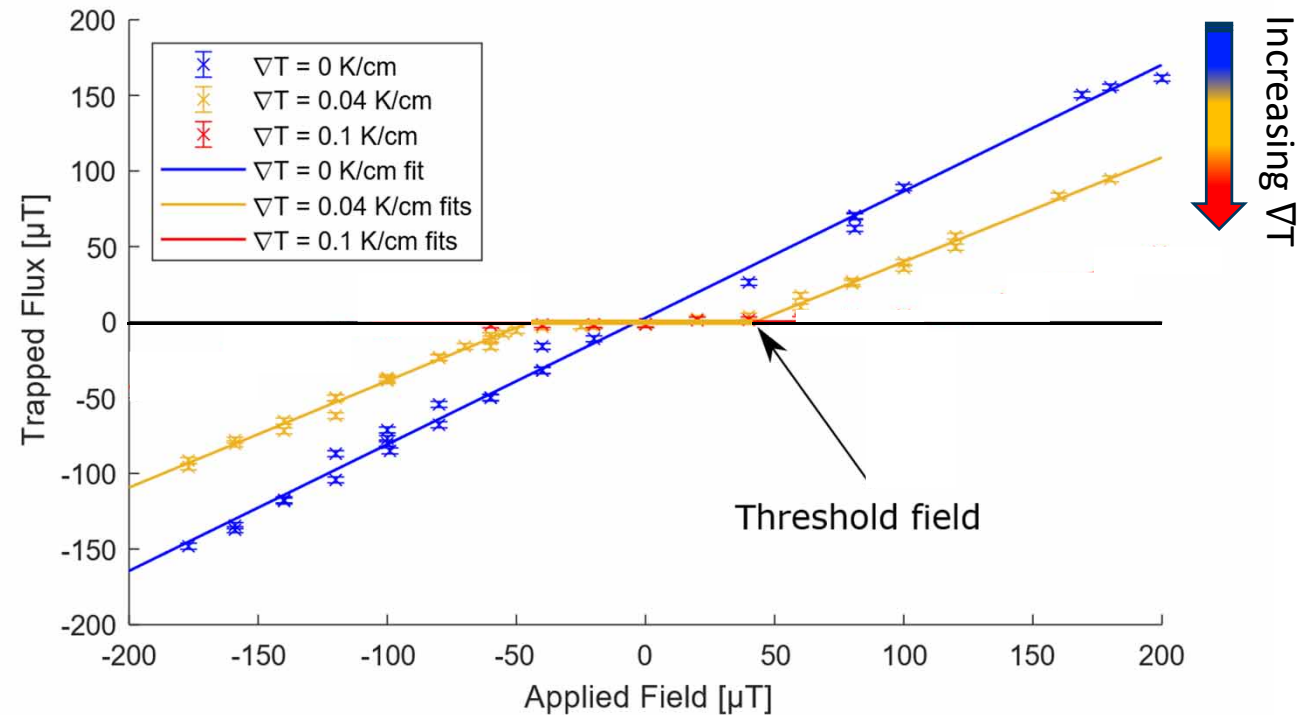
- Vary magnetic field strength with constant temperature gradient and cooldown rate
- Change Temperature gradient for different measurement runs
 - Large grain sample
 - $dT/dt = 0.07\text{K/s}$
 - $\nabla T = 0\text{ K/cm}; 0.04\text{ K/cm}; 0.1\text{ K/cm}$
- Flux is not trapped below a gradient-dependent threshold field
- Above threshold the dependence is linear
- Slope decreases with increasing temperature gradient
- This threshold behavior is not observed in fine-grain sample



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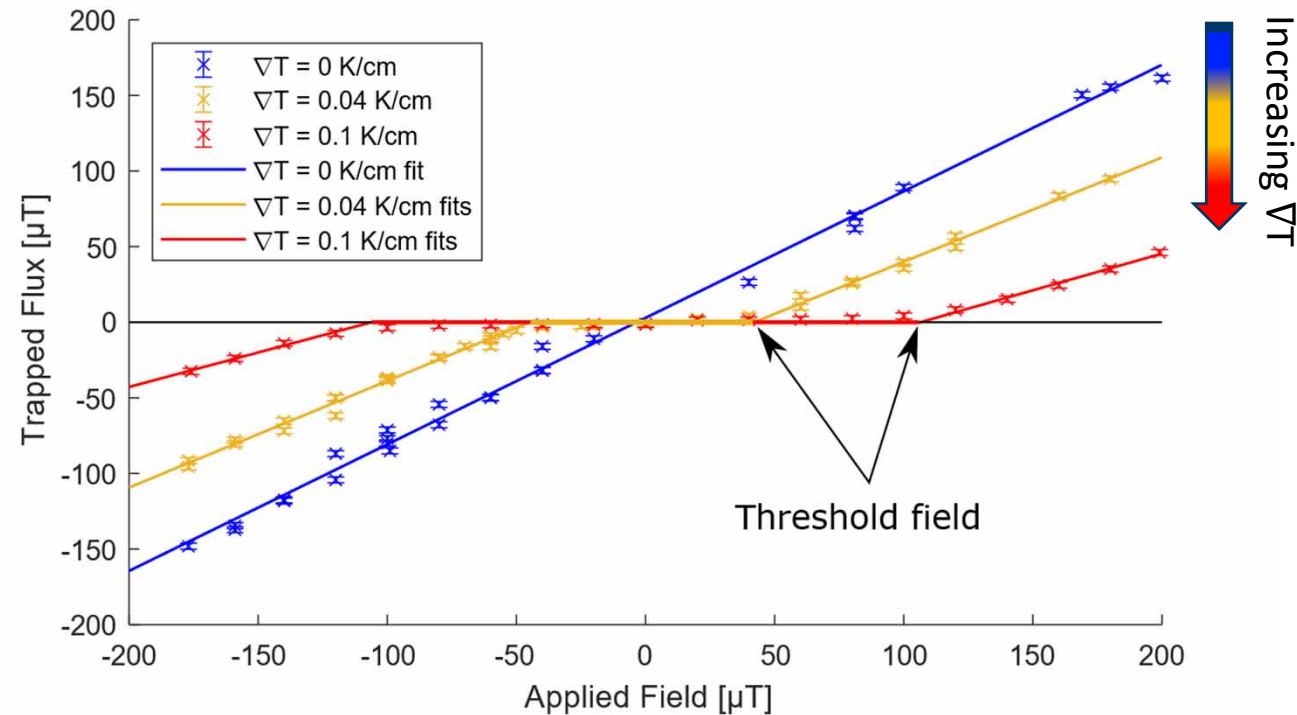
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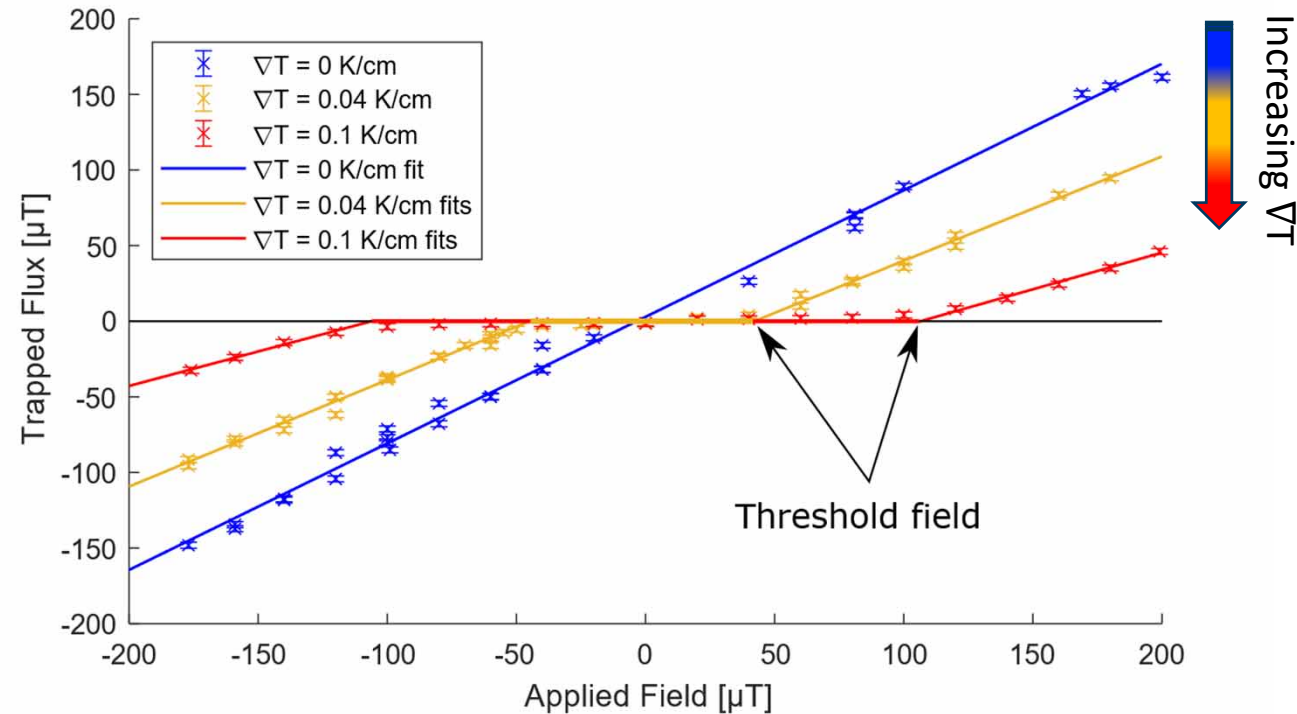
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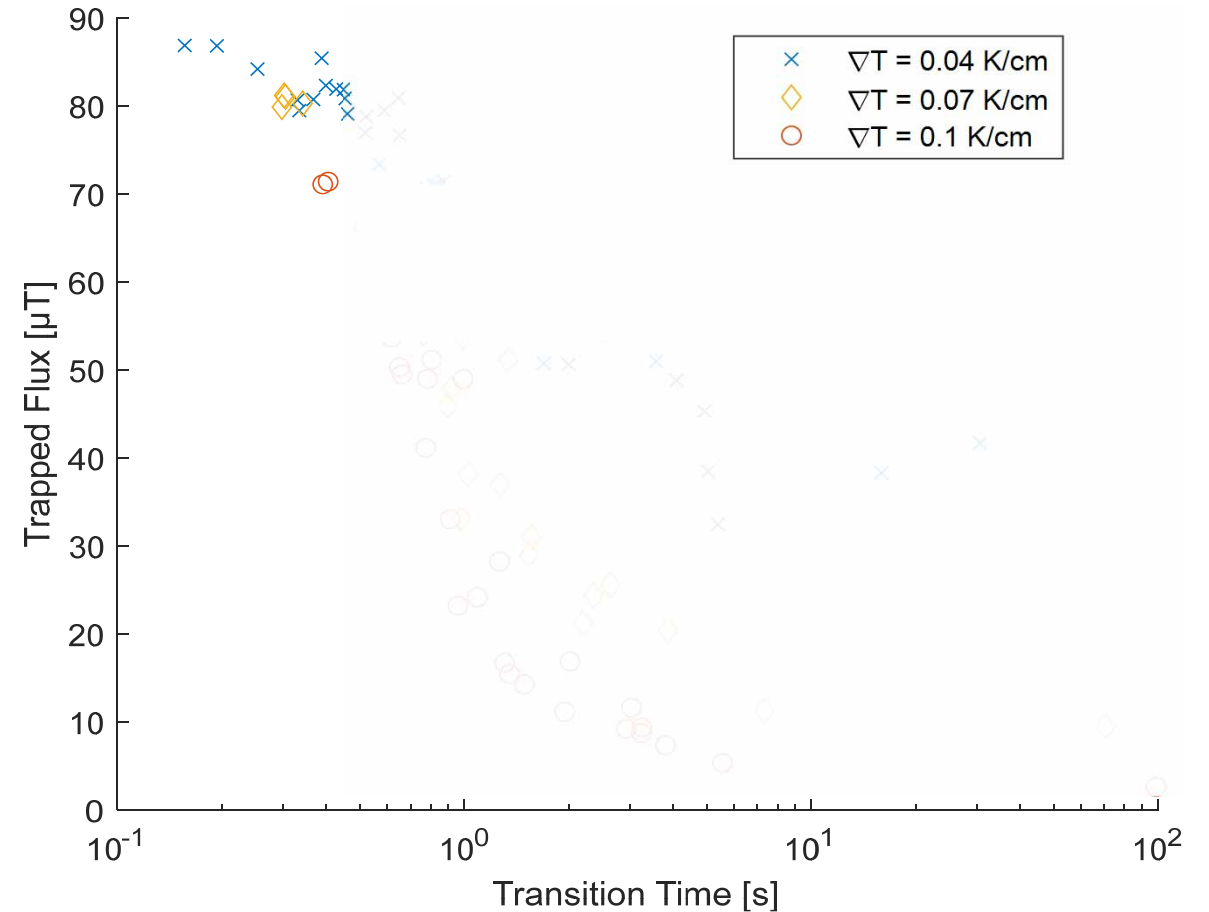


Temperature gradient dependent threshold field

TRAPPED FLUX VS COOLDOWN RATE

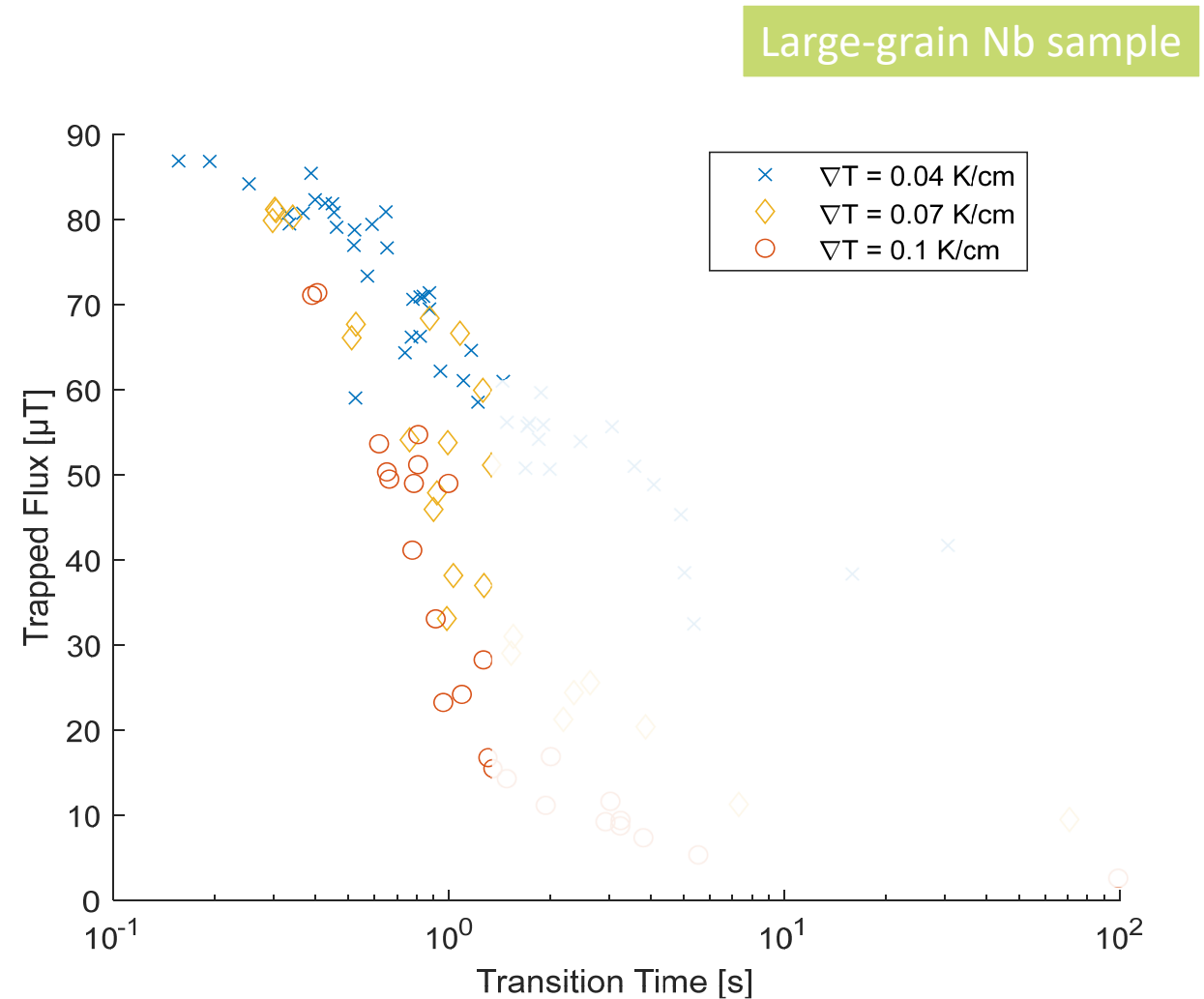
- Vary cooldown rate while keeping temperature gradient and external magnetic field constant
- Alter temperature gradient for different measurement series
 - Large grain sample
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- Increasing Trapped Flux with decreasing Transition Time
- No difference after ~10s

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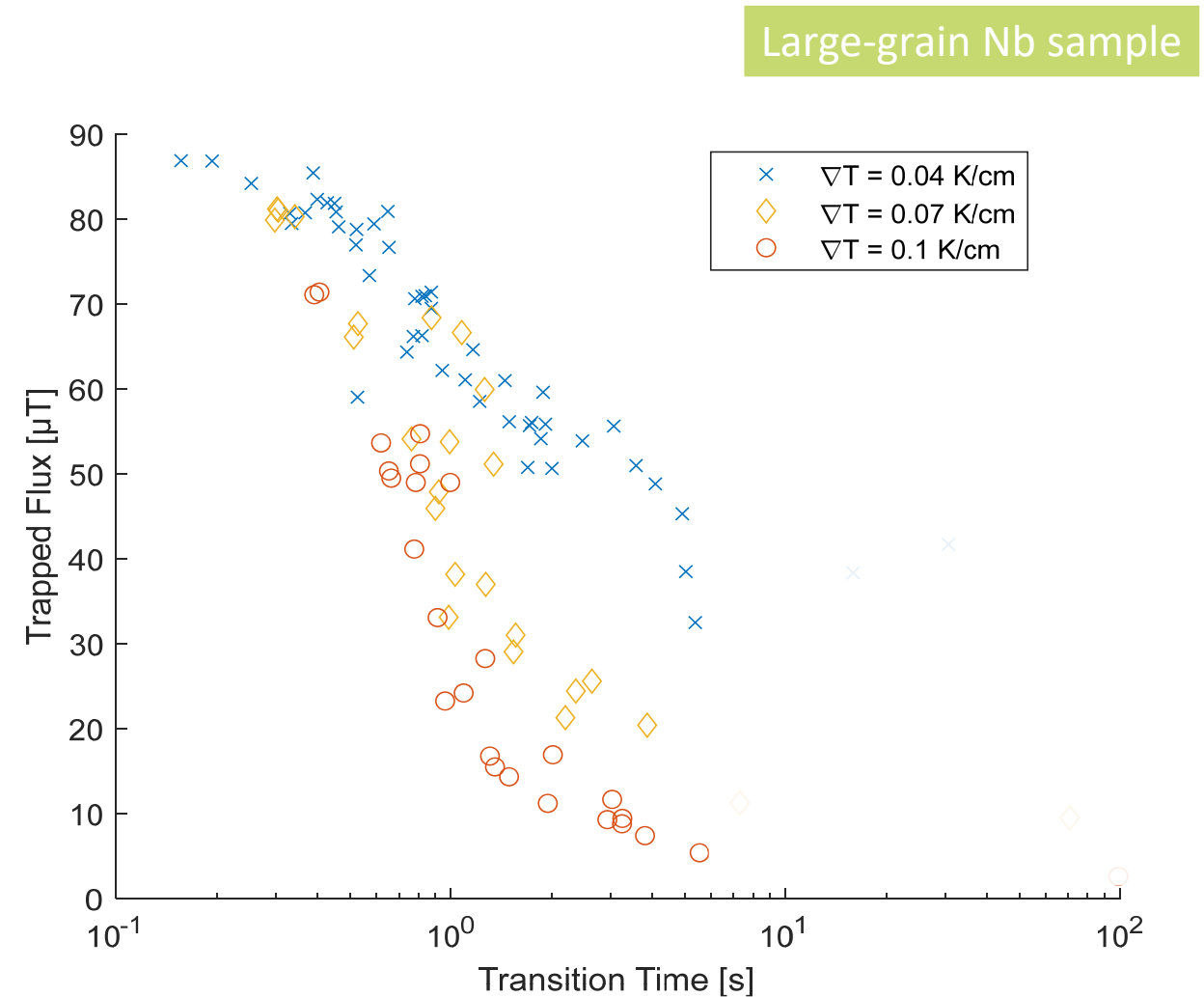
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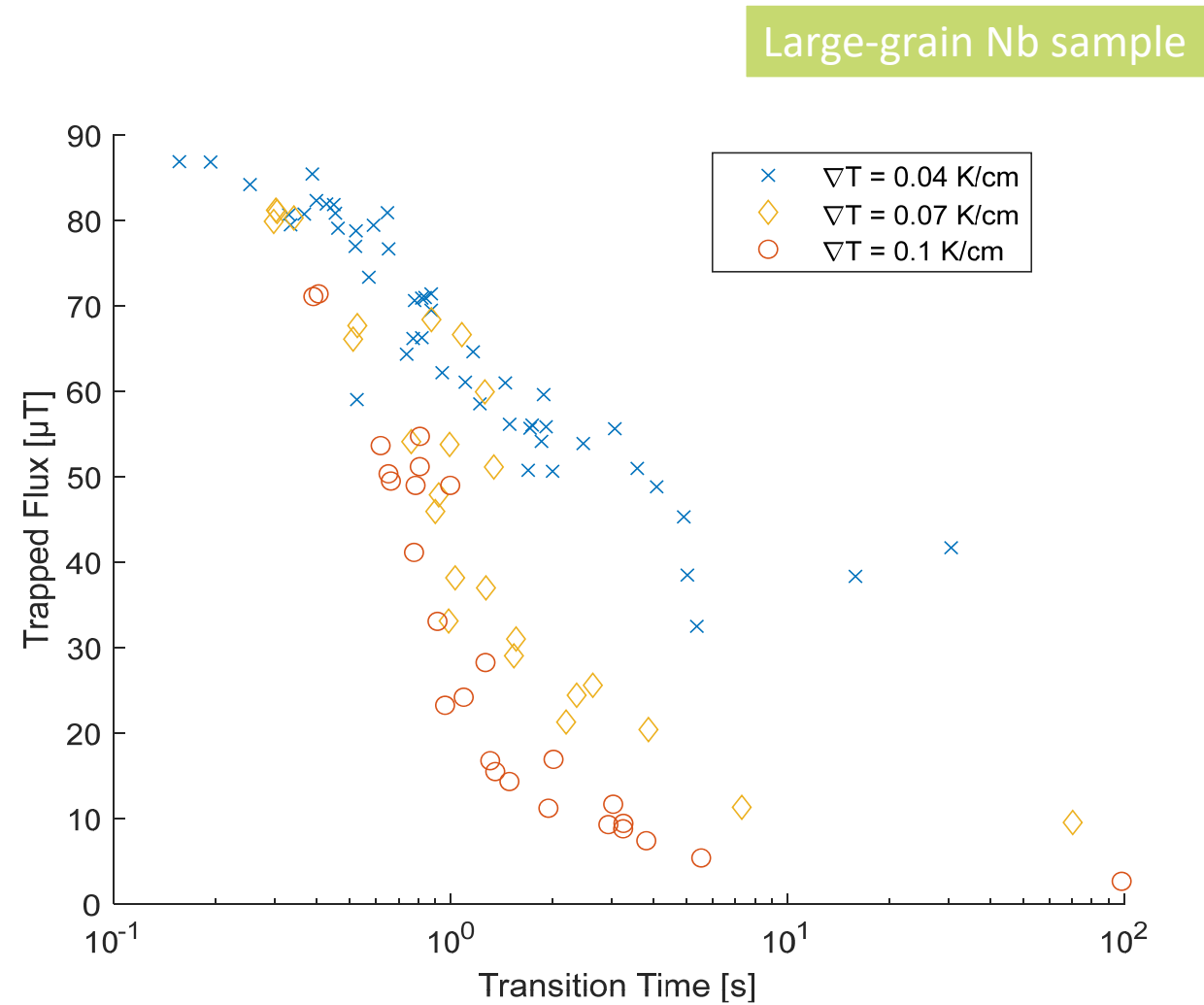
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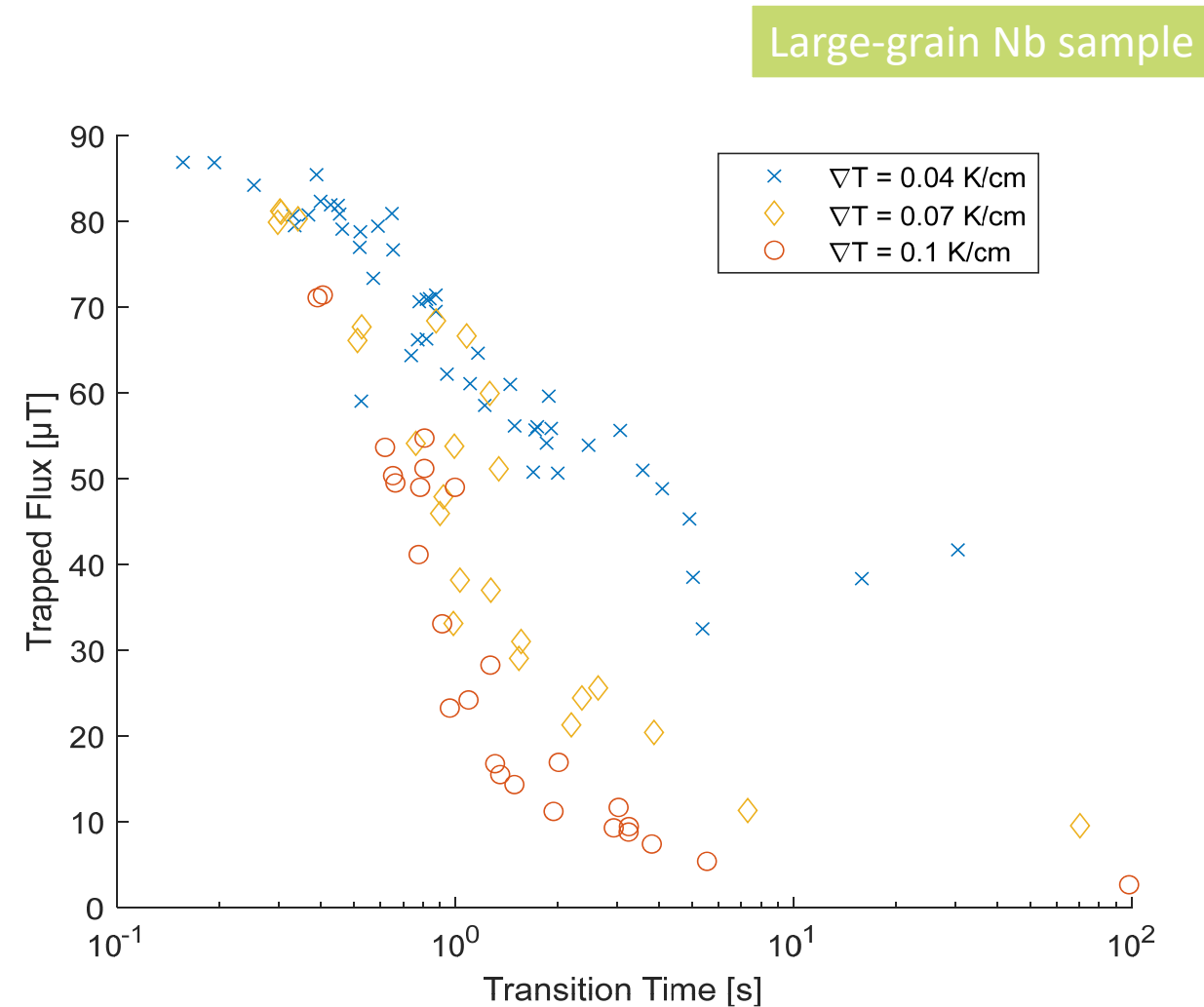
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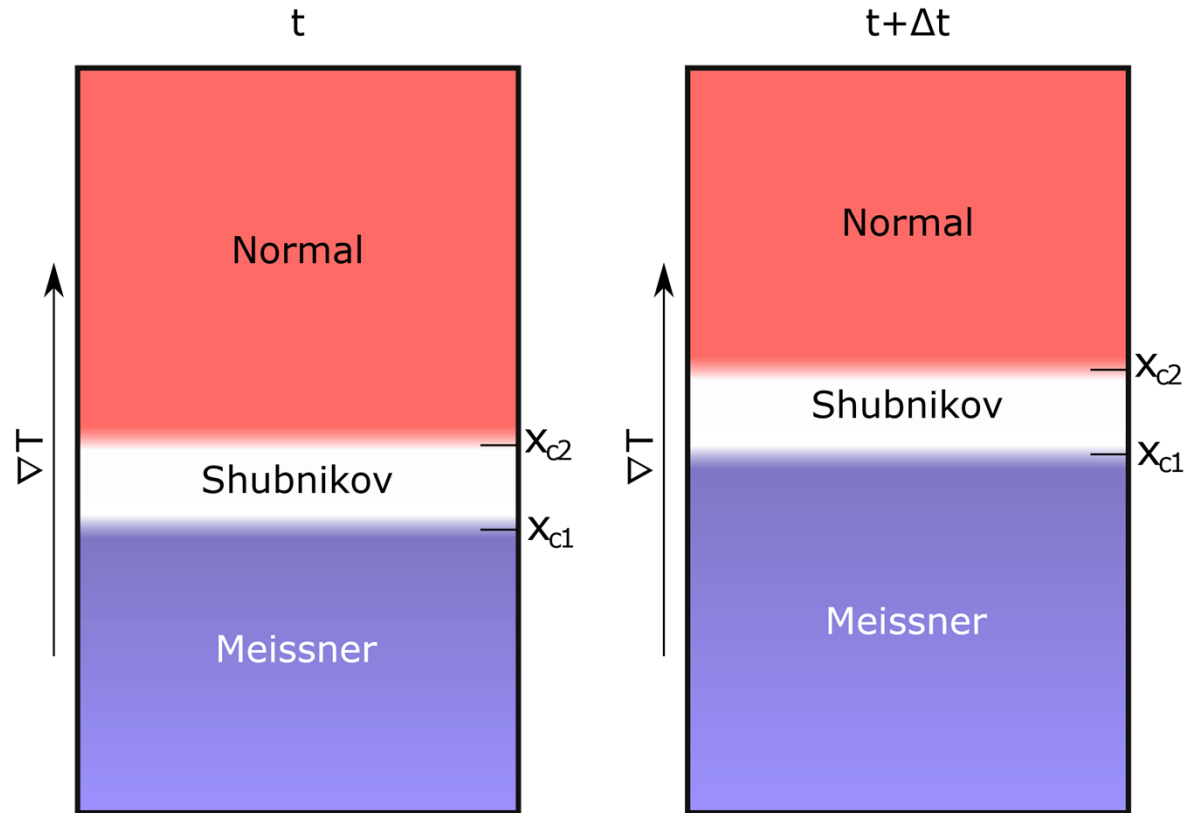
Too fast cooldowns degrade flux expulsion



BASE MODEL

- Describes trapped flux in dependence of temperature gradient and external magnetic field
- During Cooldown sample is in three states simultaneously
- Quantized flux lines establish at x_{c2}
- In Shubnikov phase flux are pushed towards Meissner state at x_{c1} by the thermal force $f_{th} = a \nabla T$ [2]
- Mechanism at x_{c1} unclear at the moment:
 - Flux lines are trapped if they are at pinning center when x_{c1} reaches them, otherwise they are expelled
 - Thermal force can push flux lines over pinning centers if $f_{th} > f_p$

More details on Poster TUPTB002



[2] R. P. Huebener, "Superconductors in a temperature gradient," *Supercond. Sci. Technol.*, vol. 8, no. 4, pp. 189–198, 1995

BASE MODEL

- Introduce distribution function $n(f_p)$ describing probability of flux line to interact with pinning center with f_p

- $\int_0^\infty n(f_p) df_p = 1$

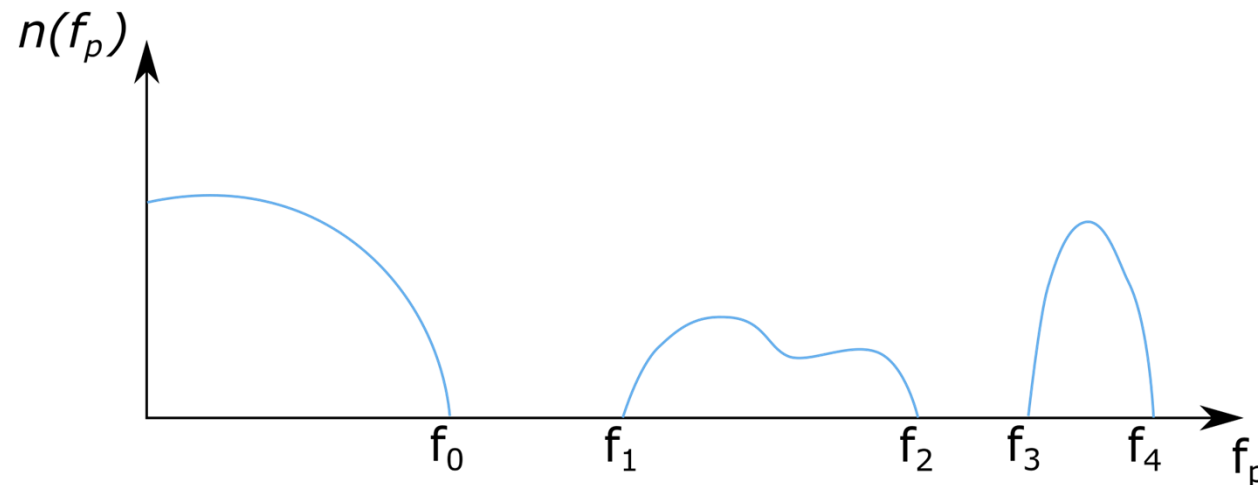
- Calculate ratio of expelled flux lines

$$r(\nabla T) = \int_{f_p < f_{th}} n(f_p) df_p$$

- Two assumptions

1. $f_0 < f_{th\ max} < f_1$

2. $n(f_p < f_0) = n_0 = const.$



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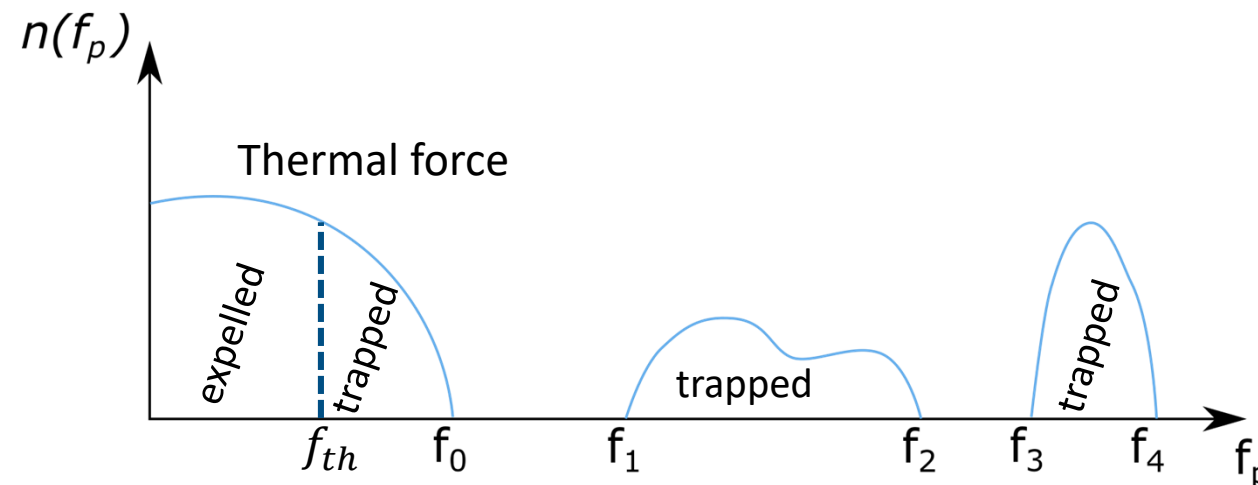
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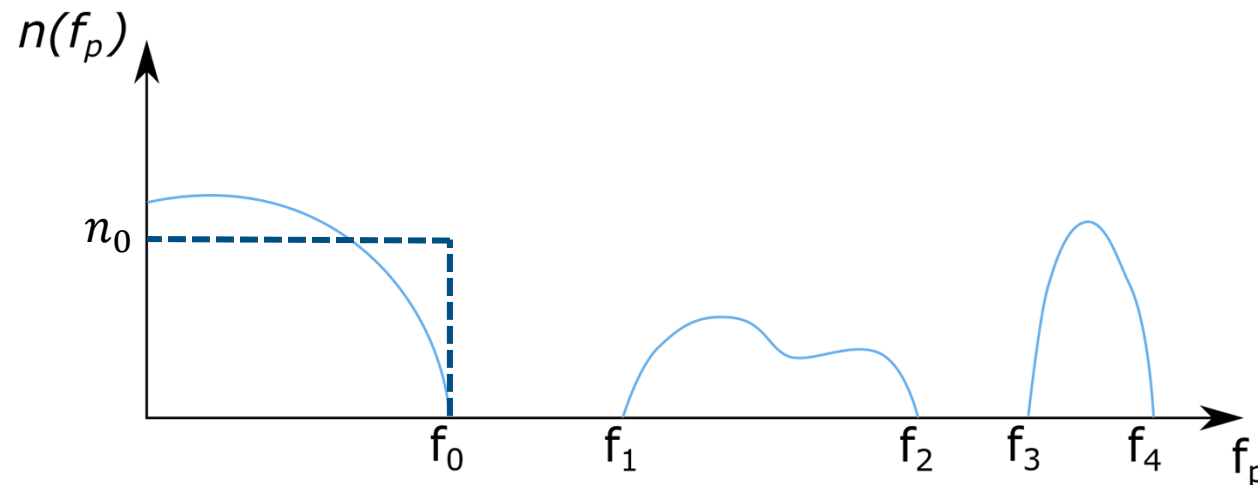
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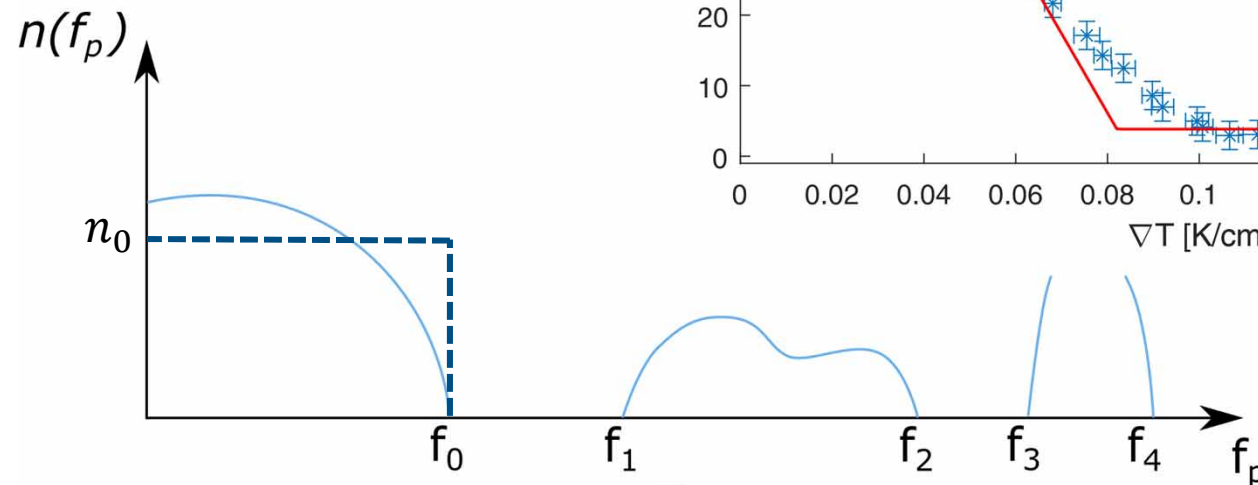
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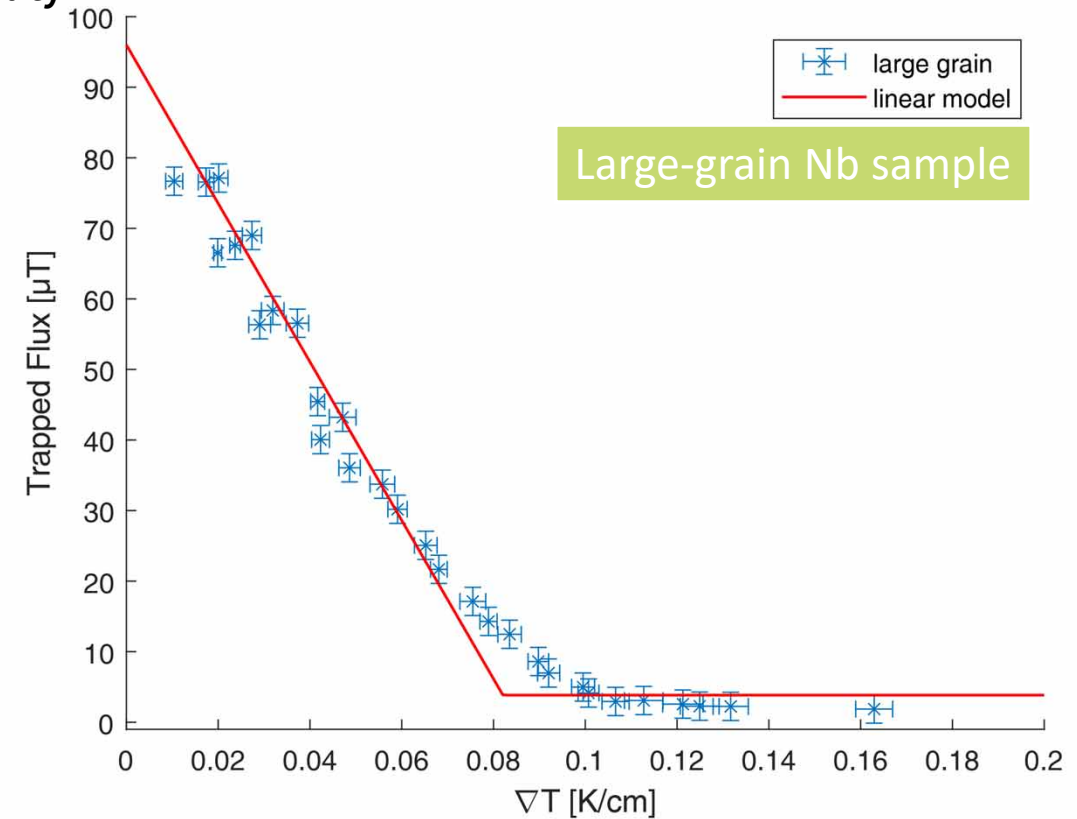
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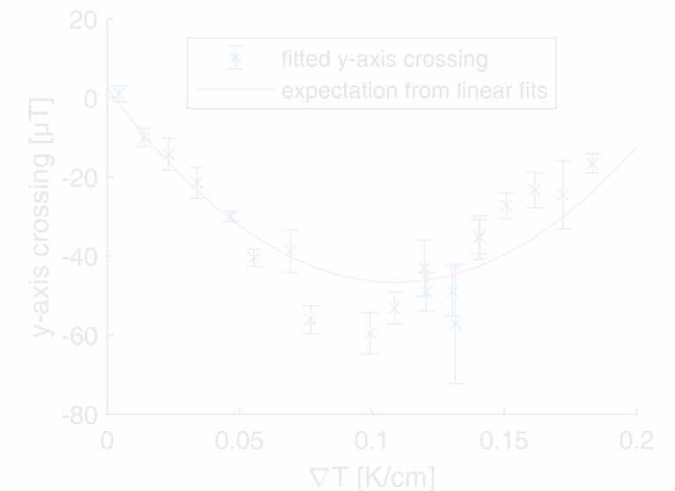
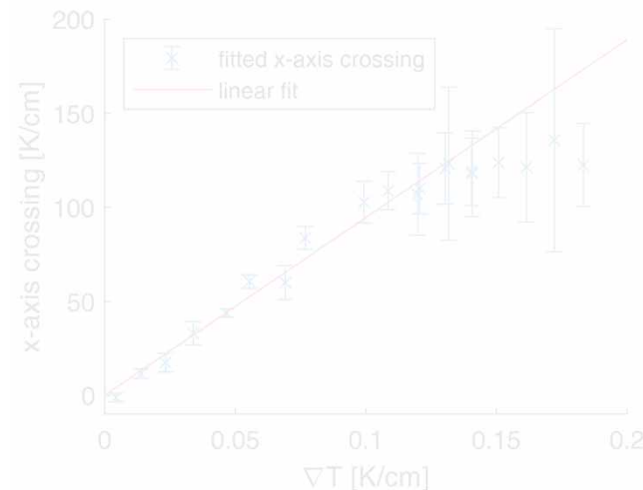
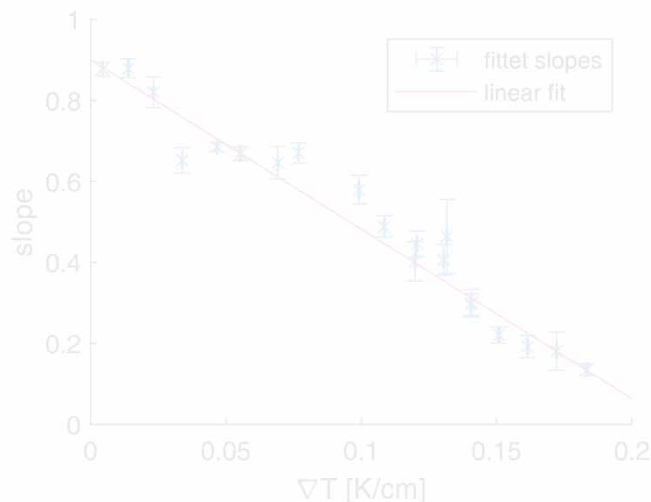
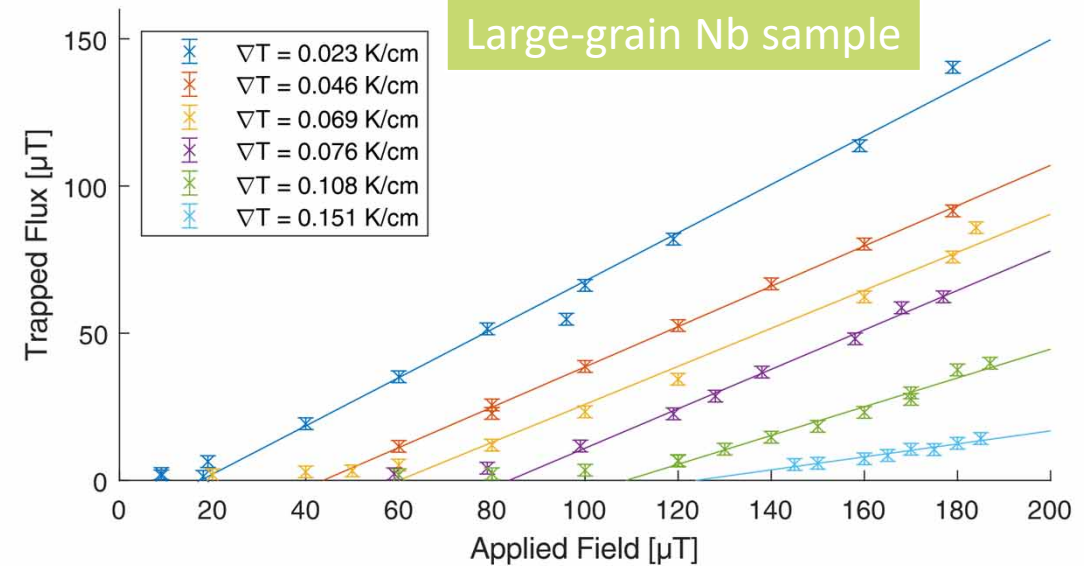
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Large-grain Nb sample

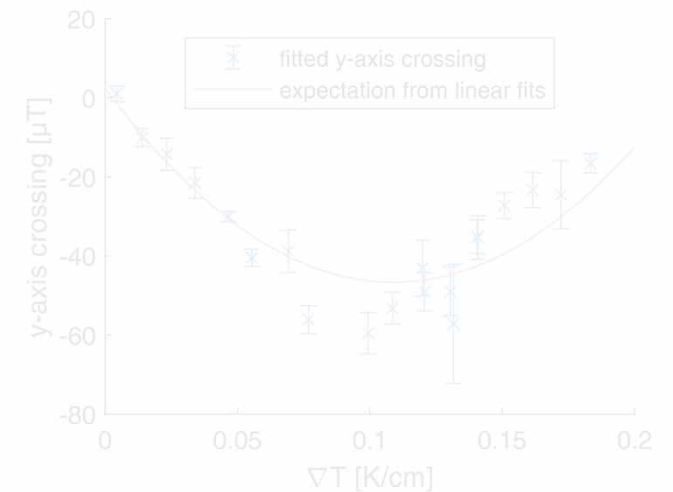
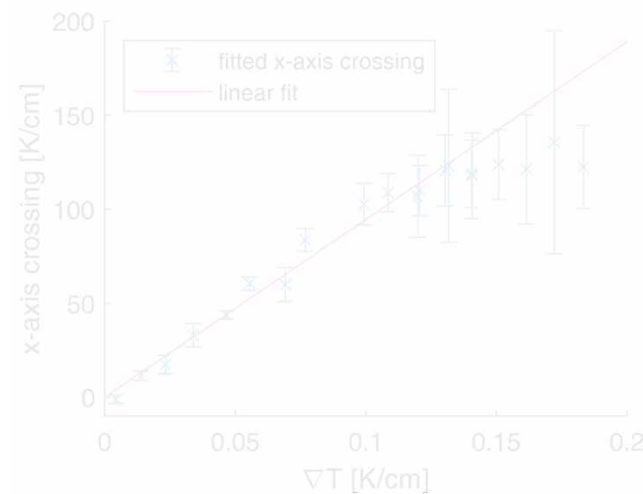
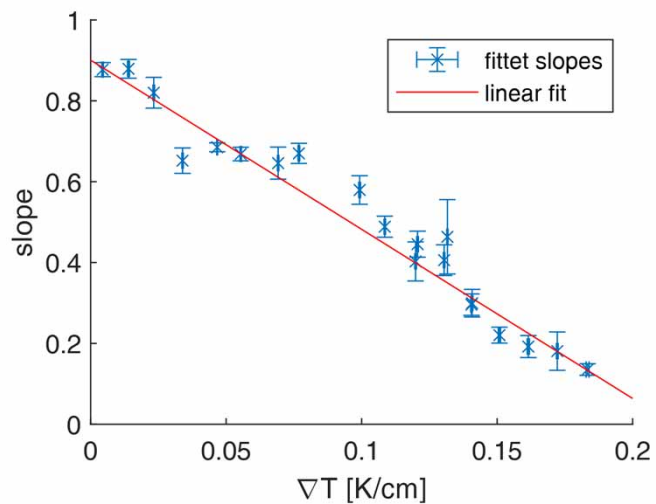
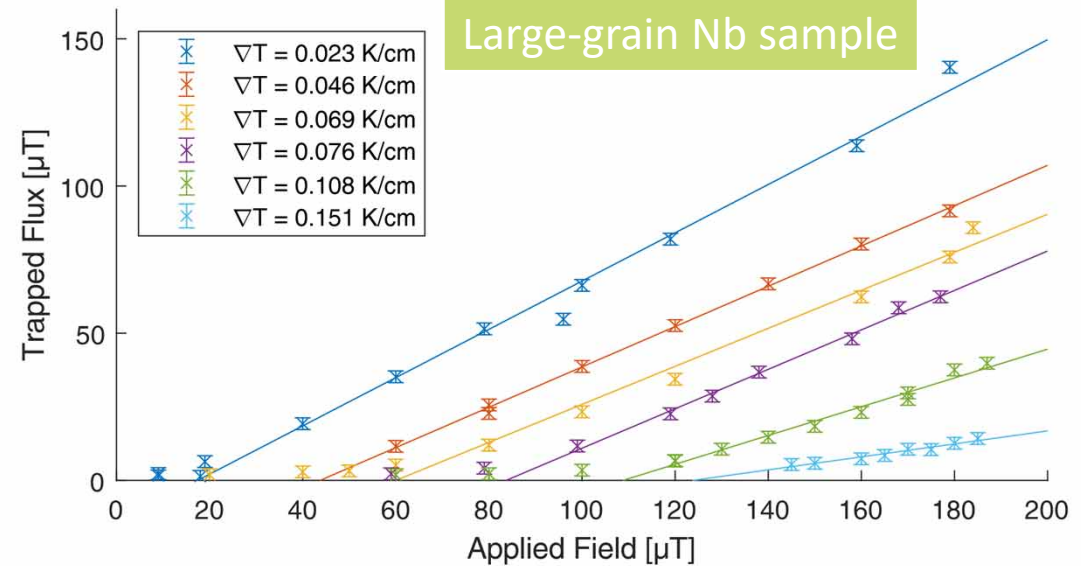
REFINED MODEL

- Linear fits of trapped flux versus external field data
- Plot slope, x-axis, and y-axis crossing versus temperature gradient
- Slope and x-axis crossing show linear dependency on temperature gradient
- => y-axis crossing must have quadratic dependency on temperature gradient



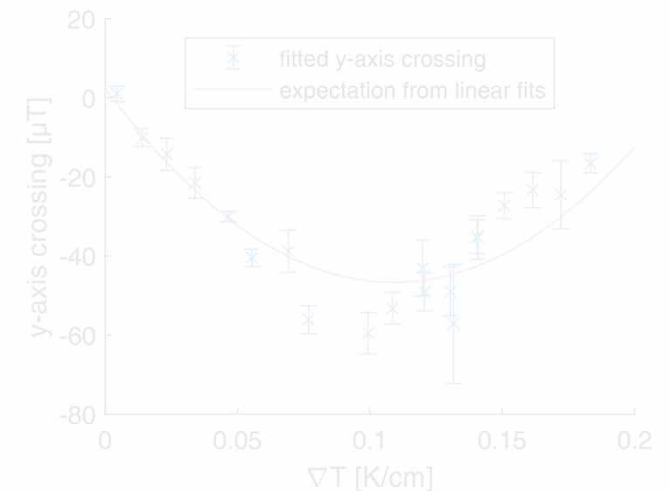
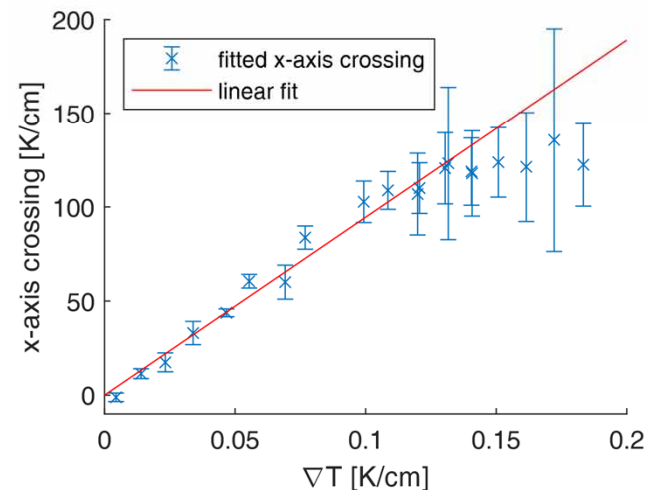
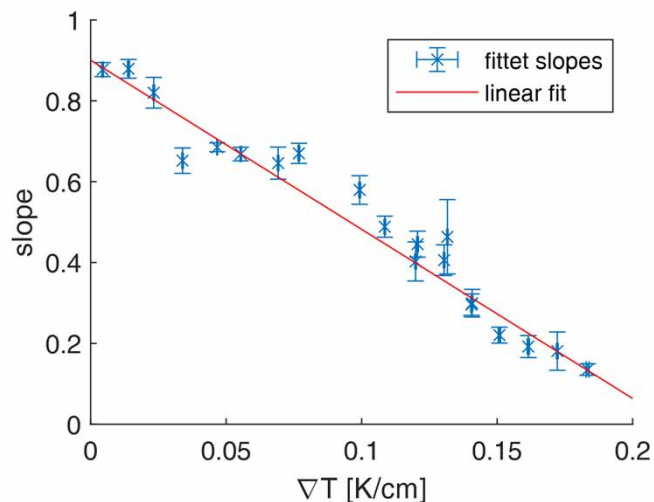
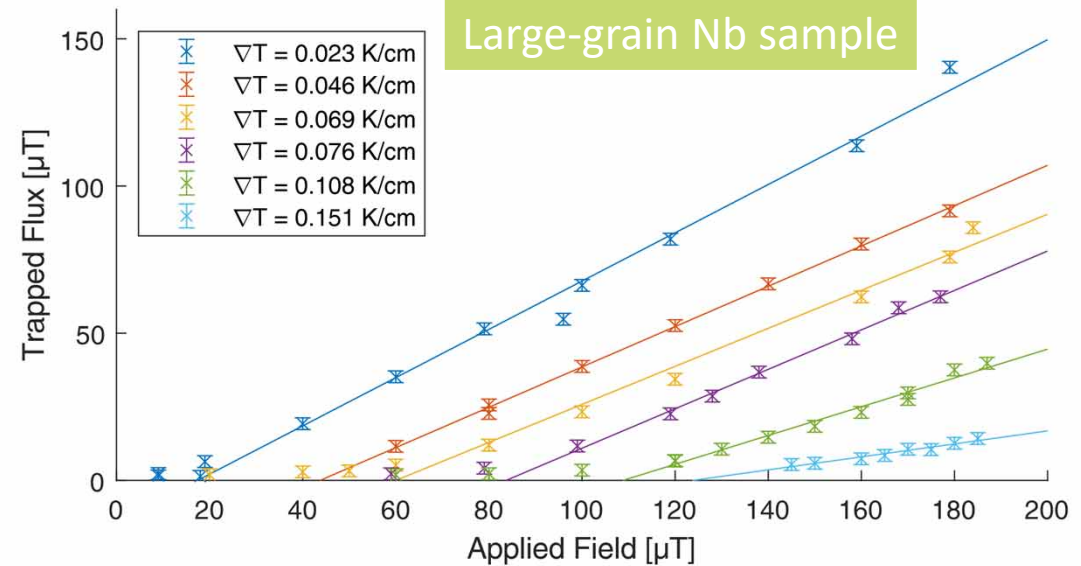
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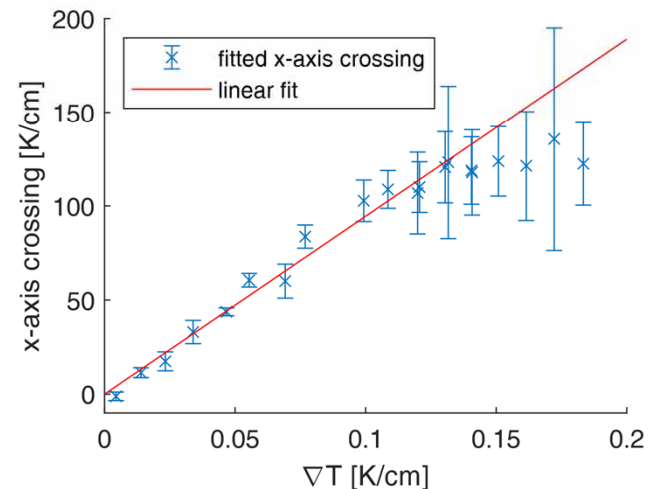
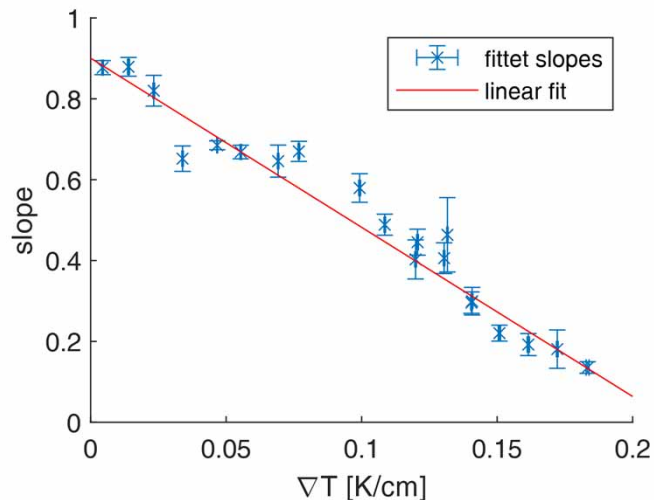
REFINED MODEL

- Linear fits of trapped flux versus external field data
- Plot slope, x-axis, and y-axis crossing versus temperature gradient
- Slope and x-axis crossing show linear dependency on temperature gradient
- => y-axis crossing must have quadratic dependency on temperature gradient

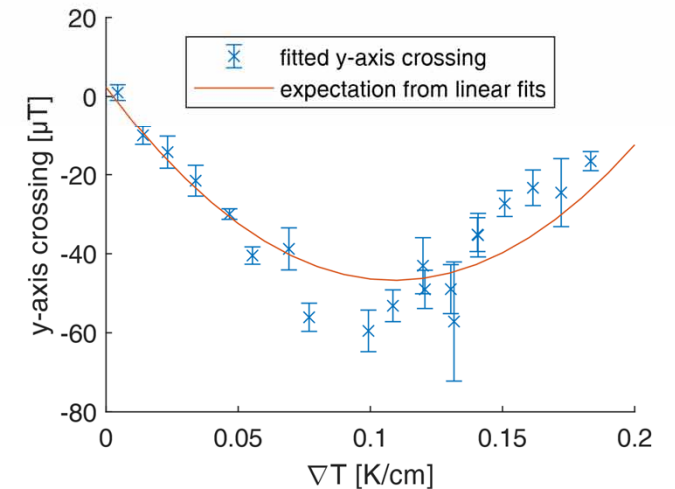
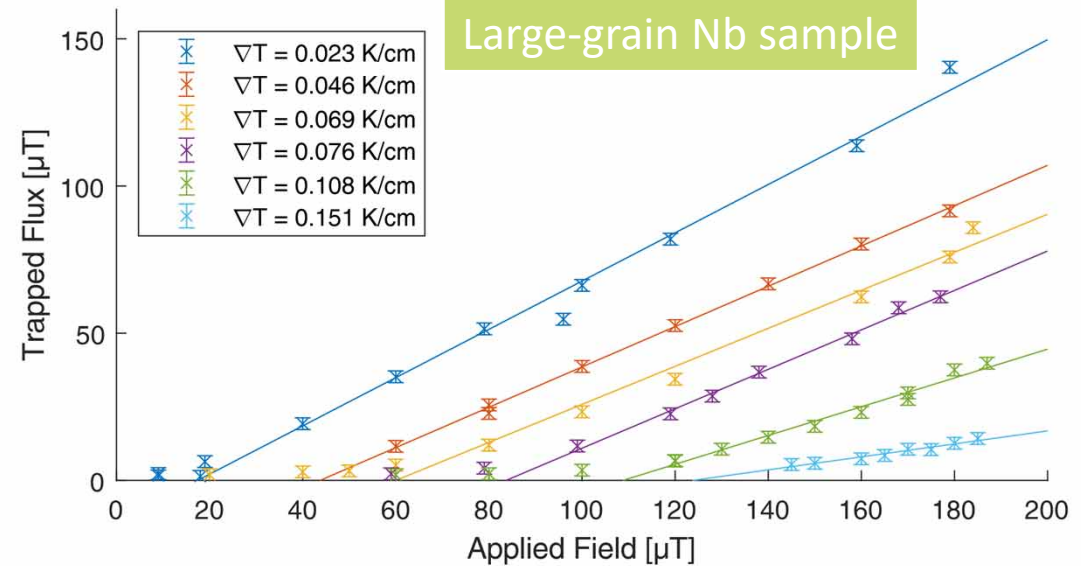


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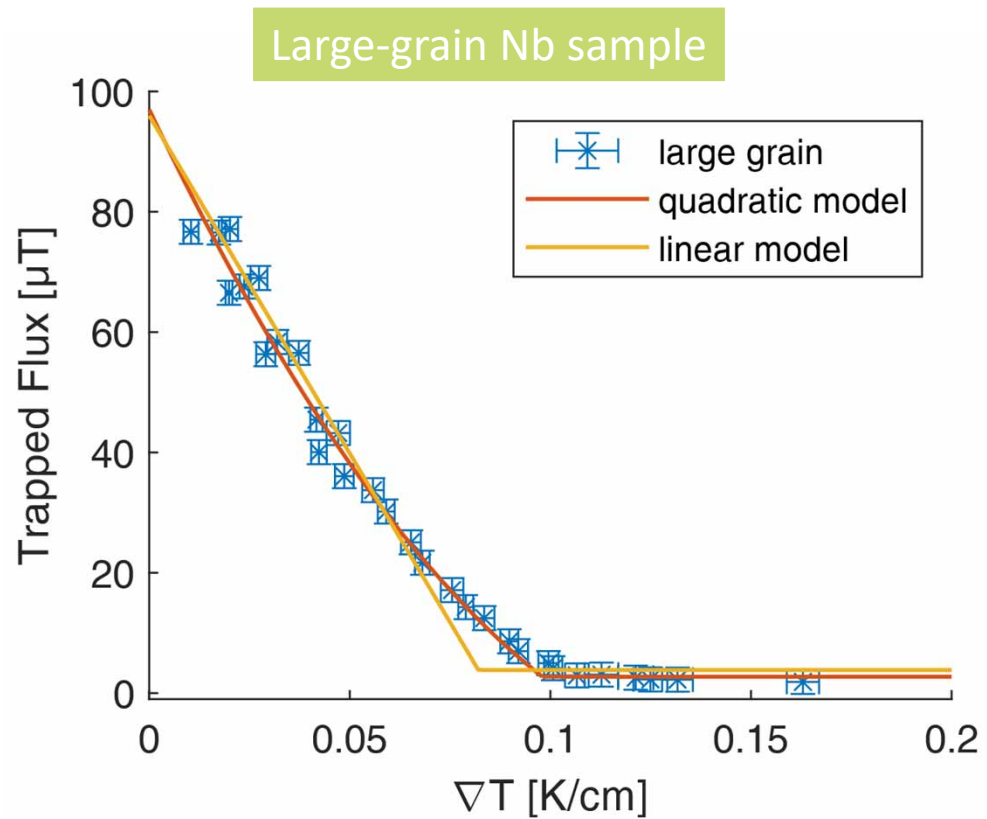
More details on Poster TUPTB002



REFINED MODEL

More details on Poster TUPTB002

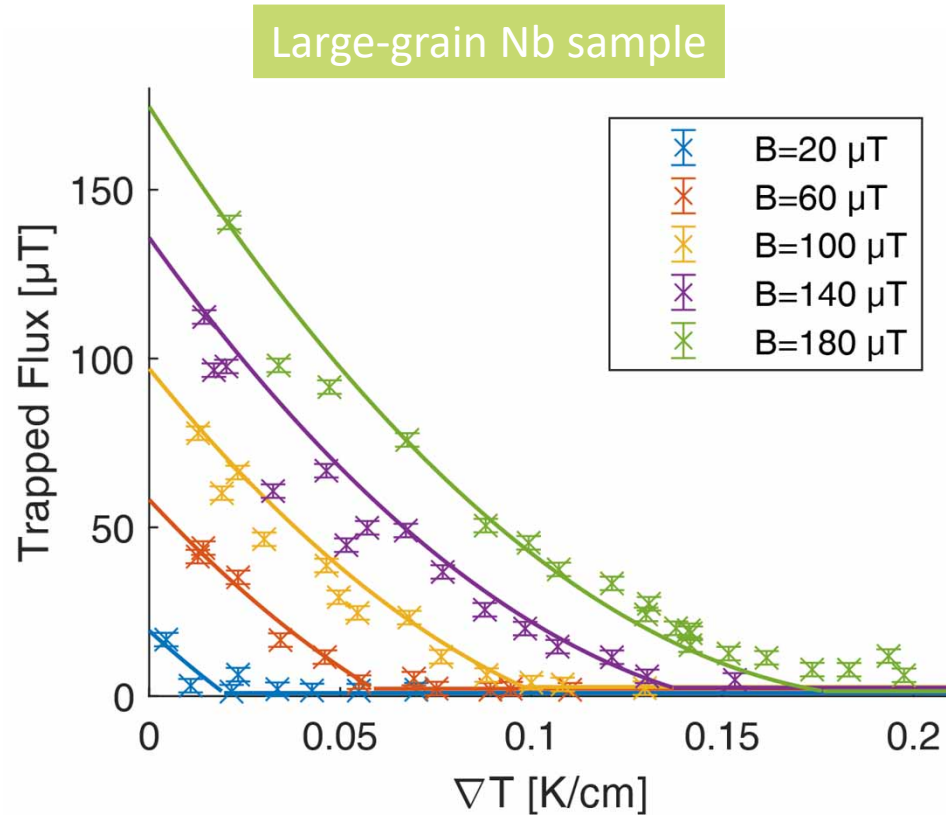
- Quadratic term results in a quadratic correction term in the model



REFINED MODEL

More details on Poster TUPTB002

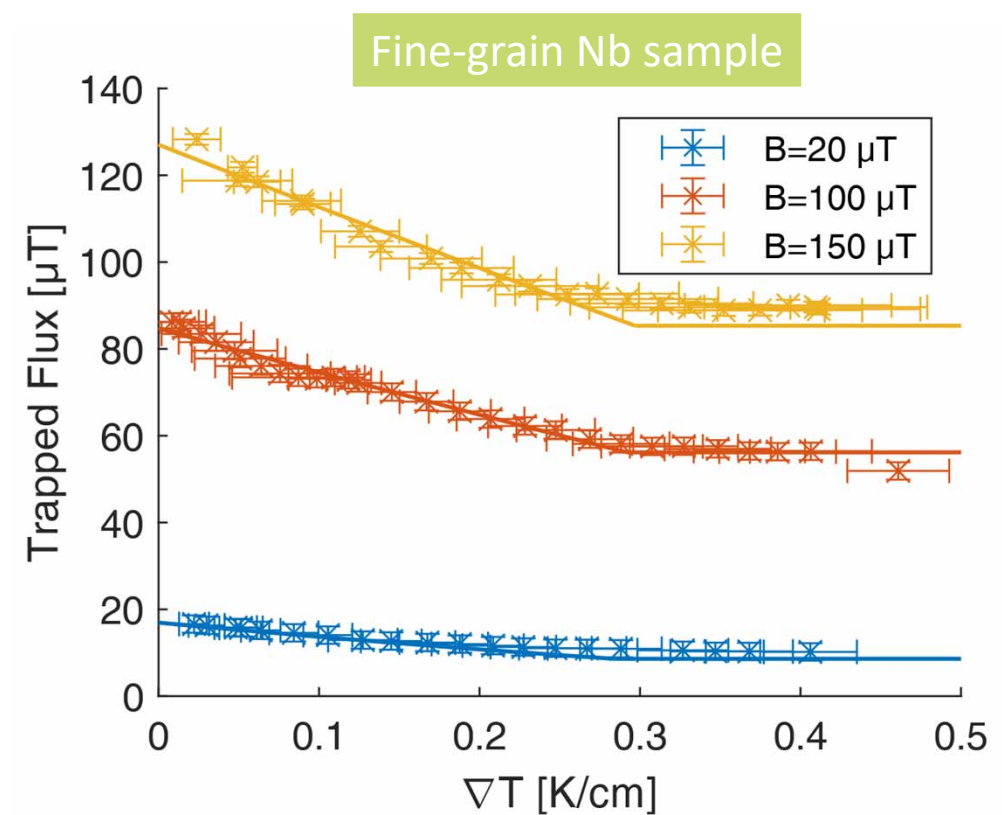
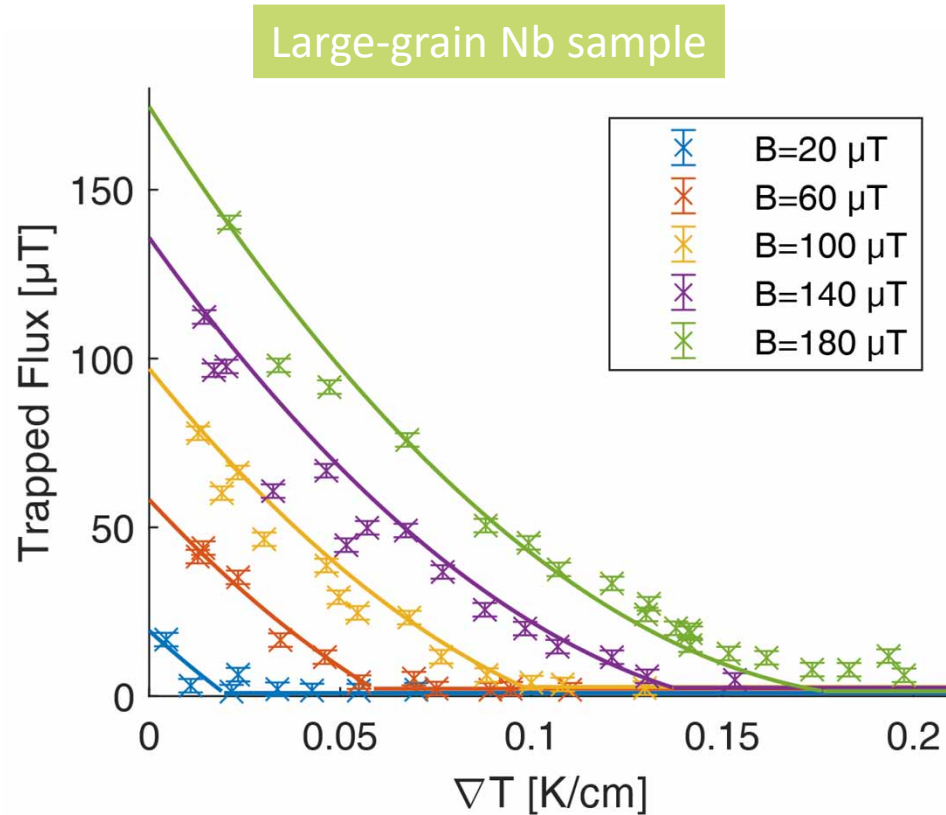
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CONCLUSION

Temperature Gradient / Material

- Better expulsion at higher gradients
- Large grain expels flux much more efficiently than fine grain
- Above 0.1 K/cm all flux is expelled in large grain sample

External magnetic field

- Depending on temperature gradient, flux is only trapped above threshold field
- Linear dependency above threshold field

Cooldown speed

- Flux needs time to exit the superconductor

Model

- Agrees well with data, and correctly predicts trapped flux at different external flux densities
- Still open questions regarding dynamics at Meissner phase front, and origin of threshold field.

OUTLOOK

- Investigate different materials (N infused Nb, Nb₃Sn, multilayer) and treatments (surface- and heat treatment)
- Develop model further and address open questions
- Develop methods to decrease trapped flux